## Geological Technics Inc. \_\_

### Report

Risk Evaluation & Appendix B Site Closure Checklist

City of Escalon Former Arco Gas Mini Mart 1305 Escalon Ave. Escalon, CA

> Project No. 750.2 May 16, 2005

> > **Prepared for:**

Mr. Doug Stidham
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**Prepared by:** 

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May 16, 2005

Project No.: 750.2

Project Name: City of Escalon (Former Arco)

Mr. Doug Stidham City of Escalon P.O. Box 248 Escalon, California 95320

Report: Site Characterization, Risk Evaluation and Appendix B Site Closure Checklist

Location: Former Arco Gas Mini Mart, 1305 Escalon Ave, Escalon, CA

Dear Mr. Stidham:

Attached is a Risk Evaluation and Appendix B Site Closure Checklist as required by the RWQCB-CVR for site closure. The Appendix B Report addresses the investigation of the extent of soil and groundwater containing petroleum hydrocarbons sourced from a former underground storage tank and/or associated plumbing located at 1305 Escalon Avenue, Escalon, California.

If you have any questions or need additional information, please contact me.

Respectfully Submitted,

Raynold I. Kablanow II, Ph.D. Vice President

cc: Lori Duncan – SJC PHS/EHD Jim Barton - CRWQCB-CVR

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1101 7<sup>TH</sup> Street Modesto, California 95354 (209) 522-4119 / Fax (209) 522-4227

# Risk Evaluation & Site Closure Checklist

City of Escalon Former Arco Gas Mini Mart 1305 Escalon Ave. Escalon, CA

> Project No. 750.2 May 16, 2005

#### 1.0 INTRODUCTION

The site is located at 1305 Escalon Ave, Escalon, California in the Highway 120/McHenry Avenue Improvement Project. Figure 1 is a vicinity map and Figure 2 is a site map. This property was previously an Arco Gas and Mini Mart.

Previous work at this site, performed between 1996 and 1999, includes two limited soil borings, soil sample analysis, and the removal of the USTs and pump islands. During removal activities, soil samples were collected which showed the presence of BTEX, TPH-G and MTBE.

On February 12 and 23, 1999 Geological Technics Inc. (GTI) drilled six boreholes, collected soil and groundwater samples (including one groundwater sample from each borehole via hydropunch methods) and tested these samples for petroleum hydrocarbons. Analytical results show the presence of BTEX, TPH-G and oxygenated fuel compounds in the soil and groundwater.

From April of 1999 through January of 2000 three groundwater monitoring wells and four vapor extraction wells were installed on the site. Soil samples collected during the drilling of these wells show low to moderate levels of BTEX, TPH-G, MTBE and TBA in MW-1. Low levels of MTBE were detected in MW-2. Soil samples collected from VEW-1 showed low levels of Xylene and MTBE.

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On June 12, 2000, GTI and Del-Tech Geo Technical (Del-Tech) performed a vapor extraction pilot test at the site. Laboratory and field test results indicate the site is conducive to remediation by vapor extraction.

On June 12, 2000, Ms. Lori Duncan of San Joaquin County Environmental Health Department (SJCEHD) requested in writing that a work plan be prepared to define the lateral and vertical extent of the groundwater plume at the site. On June 29, 2000, GTI prepared a work plan proposing the installation of two water table monitoring wells and one deep, discretely screened monitoring well. Ms Duncan approved the work plan on July 7, 2000. The work was performed during the week of October 16, 2000.

On January 30, 2001, GTI prepared and submitted the *Corrective Action Plan (Revised) Vadose Zone Remediation*. The CAP discusses GTI's proposed methodology for mitigation of the documented petroleum hydrocarbon contamination at the site by vapor extraction. The CAP also discusses the confirmation testing outlined in this work plan. Ms Duncan approved the CAP, as submitted, in a letter dated April 02, 2001.

In February 2002 the soil vapor extraction (SVE) system was initiated and has operated for approximately one year. On January 21, 2003, GTI submitted the *Vapor Extraction Treatment System Monitoring Report*. The report indicated that approximately 50% of the petroleum hydrocarbons contained in the subsurface have been removed, the groundwater at this site is free of petroleum hydrocarbon contamination, and possibly as much as 600 gallons of gasoline may remain in the vadose zone. The report also recommended that the site be considered for closure.

In a letter dated February 18, 2003, SJCEHD requested that the well extraction cycle be utilized to address lower screen intervals and that GTI may consider switching methods of contaminant destruction, such as changing to carbon canisters to lower operational costs.

On March 28, 2003, GTI submitted the *Additional Site Characterization – Soil Borings Work Plan*. Ms Duncan approved the work plan, with reservation, in a letter dated April 8, 2003. The soil borings were advanced on September 5, 2003 and GTI submitted the resulting *Interim Soil Investigation Report* on October 2, 2003. As per the April 8, 2003 SJCEHD directive, the SVE system was restarted on December 9, 2003 and ran until January 14, 2004.

A new vapor extraction – granulated activated carbon (SVE-GAC) system was installed during the summer of 2004. The SVE-GAC was started on September 24, 2004 and ran until April 12, 2005. The SVE-GAC was not operational, due to repairs, for three weeks between December 2004 and January 2005.

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#### 2.0 HYDROGEOLOGIC SYSTEM

#### 2.1 Regional Structure

The COE site is located in the northwest quarter, of the northwest quarter of Section 4, T2S, R9E, related to the Mount Diablo B&M, on the United States Geological Survey (USGS) topographic map, Escalon Quadrangle, California, 7.5 minutes series. A review of the USGS Topographic Map reveals that the elevation of this site is approximately 115-feet above mean sea level (AMSL).

The site is located on the gradually sloped floor of the northern San Joaquin Valley. The geologic composition of the area is characterized as fluvial deposits of the San Joaquin - Sacramento River delta system that overlay continental rocks and deposits derived from erosion of the Sierra Nevada Mountain Range located approximately 50 miles northeast of Modesto.

The southwest tilting Sierra Nevada fault block underlies the northern San Joaquin Valley area. Overlying the consolidated rocks are unconsolidated sediments. The lower consolidated batholithic and metamorphic rocks are poorly transmissive; however, the overlying sedimentary layers are often quite permeable. These unconsolidated layers include Pliocene/Pleistocene age continental deposits, Pleistocene age lacustrine and marsh deposits, and Holocene older and younger alluviums and flood-basin deposits.

#### 2.2 Regional Stratigraphy

The following information comes from the United States Department of Agriculture – Soil Conservation Service (USDA). *Soil Survey of San Joaquin County, California* (1992) indicates the area surrounding the COE site is predominately made up of one general soil type:

 DELHI – VERITAS – TINNIN: A gentle 0 to 2 percent slope; moderately well drained to somewhat excessively drained, coarse textured and moderately coarse textured soils that are deep to a cemented hardpan or are very deep; on dunes, alluvial fans and low fan terraces.

The USDA *Soil Survey of San Joaquin County, California* (1992), states the area beneath the COE is categorized as Delhi loamy sand with the following description:

• Delhi loamy sand – 0 to 2 percent slopes. Very deep, somewhat excessively drained, nearly level soil on dunes. It formed in wind-modified alluvium derived from granitic rock sources. The average annual precipitation is about 11-inches, the average air temperature is about 60° F.

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#### 2.3 Site-specific Hydrogeology

#### 2.3.1 Lithology and Soil Characteristics

- Top two feet of the site appears to be backfill materials comprised of gravel and sand
- Brown, poorly sorted, sand from 5 to 10 feet bgs, which overlies a dry, light brown, silt unit between 10 and 20 feet bgs
- The geology from 20 to 30 feet bgs consists of various layers of grey colored silt and sand
- The predominant geology between 30 and 45 feet bgs is comprised of a buff color, poorly sorted sand containing some clasts greater than 1 centimeter in size
- Grey silt and sandy silt layers were noted between 43.5 and 50 feet bgs
- Sand characterizes the 50 to 55 foot interval buff and well sorted at 50 feet bgs grading down to brown and poorly sorted at 55 feet bgs

A site map showing the locations of streets, structures, wells, and other site-related details is attached as Figure 2.

#### 2.3.2 Groundwater Bearing and Gradient

Groundwater bearing and gradient data has been collected since April of 2000. The historical groundwater information for the site is as follows:

- Average groundwater elevation is 56.71 AMSL
- Average depth to groundwater is 62.67 feet below grade
- Average bearing is N73°W
- Average gradient is 0.0019 ft/ft

#### 2.3.3 Vertical Groundwater Gradient

The vertical gradient has been calculated using the MW-1/MW-101 pair. The vertical gradient is generally negative (a downward direction). However, it has been insignificant due to a near zero head difference between MW-1 and MW-101. The historical average vertical groundwater gradient is -0.0039 ft/ft.

#### 2.3.4 Average Groundwater Velocity

The lithology at the COE site will be divided into four general layers for the purposes of calculating the average horizontal groundwater velocity (AHGV).

- o Layer 1 consists of silts and sands from 5- to 30-feet bgs
- o Layer 2 is primarily sand with some larger clasts from 30- to 45-feet bgs
- o Layer 3 is primarily silt from 45- to 50-feet bgs
- o Layer 4 is primarily sand from 50- to 70-feet bgs.

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The average depth to groundwater at the site suggests only Layer 4 will contain groundwater in a saturated state. The following calculations are based on the following equation:

v = K i/n

where:

v is the average horizontal groundwater velocity (AHGV) K is the average hydraulic conductivity i is the average hydraulic gradient, n is the effective porosity.

K and n values are estimated from tables in <u>Groundwater and Wells 2<sup>nd</sup> Edition</u> (Driscoll, F.G., 1986).

- The AHVG of Layer 1 is estimated to be approximately 0.065 to 6.5 ft/yr.
- The AHVG of Layer 2 is estimated to be approximately 5.7 to 2,850 ft/yr.
- The AHVG of Layer 3 is estimated to be approximately 5.6E10<sup>4</sup> to 0.057 ft/yr.
- The AHVG of Layer 4 is estimated to be approximately 0.758 to 75.8 ft/yr.

#### 3.0 APPENDIX B SITE CLOSURE CHECKLIST

#### 3.1 Receptor Well Survey

A sensitive receptor survey was performed in August of 2000 encompassing a 2000-foot radius around the site. The following conclusions are discussed in the *Well Receptor Survey Report* – November 14, 2000:

- Two municipal wells (Escalon City Wells) were documented at distances greater than 1,600 feet.
- Escalon High School staff indicates that an irrigation well is present on the school property, but domestic use is provided by municipal water supply.
- Two DWR well logs are included for Fisk Avenue. The addresses of these residences' could not be confirmed, however all of the residences in the area are serviced by City of Escalon municipal water supply. If these two wells still exist, they are probably not used for drinking water purposes.

#### 3.2 Non-Contamination Maps and Cross-Sections

- Figure 1: Vicinity Map showing roads, highways and waterways adjacent to the property.
- Figure 2: Site Map showing buildings, roads, lines of section, monitoring well locations, soil boring locations, former dispenser and former tank locations.
- Figure 3: West to East Lithological Cross-Section (A-A') showing subsurface features and lithology.

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Figure 4: North to South Lithological Cross-Section (B-B') – showing subsurface features and lithology.

Figure 5: Groundwater Elevation Contour (February 16, 2005)

Figure 6: Rose Diagram – showing historical groundwater elevations, gradients and bearings.

#### 3.3 Tabulated Groundwater Elevations, Gradient and Bearing

Historical groundwater elevations, gradients and bearings are summarized on Table 1 of Appendix A. The average groundwater bearing is N73°W with an average gradient of 0.0019 ft/ft.

Vertical groundwater calculations are summarized on Table 2 of Appendix A. Vertical gradients are historically negative and approximately one order of magnitude less than the horizontal gradients.

#### 3.4 Tabulated Analytical Data

Table 3: Summary of Soil Analytical Data from Tank and Trench Samples

Table 4: Summary of Soil Analytical Data – Soil Borings and Monitoring Wells

Table 5: Summary of Historical Groundwater Analytical Data

Table 6: Summary of Historical Groundwater Parameters

Table 7: Mass Balance Calculations (2001)

Table 8: Mass Balance Calculations (2005)

Table 9: Summary of TPH-G Removed by Internal Combustion System

Table 10: Summary of TPH-G Removed by Soil Vapor Extraction & Carbon Filtration

#### 3.5 Contamination Contours and Cross-Sections

Figure 7: Site Map with Soil Excavation

Figure 8: Soil Contamination Contour (TPH-G) showing Lines of Section used in Soil

Plume Cross-Sections

Figure 9: Soil Plume (TPH-G) Cross-Section C-C'

#### 3.6 Contaminant Mass Estimate Calculations

#### 2001 Mass Estimate

A preliminary contaminant mass estimate calculation was performed and submitted in GTIs: *Revised Corrective Action Plan – Vadose Zone Remediation* dated February 26, 2001. The February 2001 report estimated approximately 1,600 gallons of TPH-G was present in the soil at the site (Table 7). These calculations were very liberal using thickness of 25-feet to calculate mass. October 2003 soil investigation activities suggest the heaviest contaminated zone is likely 15-feet thick.

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#### 2003 Mass Estimate

Still being liberal, recalculating the original mass using a 20-foot thick zone of heavy contamination suggests that, prior to vapor extraction activities, there was approximately 1,248 gallons of TPH-G present in the soil at COE. Analytical results from soil borings advanced during the October 2003 soil investigation suggest that the contaminant concentrations have been greatly reduced.

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The October 2003 soil samples suggest that soil vapor extraction and natural attenuation have been effective at the site. Vapor extraction remedial activities have removed approximately 1,013 gallons of TPH-G from the site as discussed in Section 3.7. If we assume that 10% of the original estimate has undergone natural biodegradation, this would account for an additional 124.8 gallons of TPH-G removed. These calculations suggest a total of 1,138 gallons of TPH-G has been removed and approximately 110 gallons remain in the soil. The calculation suggests approximately 90% of contaminant mass has been removed since site investigation activities began in 1996.

#### 2005 Mass Estimate

After several years of remedial activities at the COE site, the revised contaminant mass estimated calculations show approximately 56 gallons of TPH-G remain in the soil (Table 8).

Figure 8 shows the soil contamination plume and a "mass balance" line of section. Figure 9 shows a cross sectional view of TPH-G contamination remaining at the site using the following information and assumptions:

- The plume is divided into three contamination zones.
- Each zone is assumed to be roughly cylindrical in shape.
- Concentrations in the zones are an average of samples collected from those zones.
- Area is determined by map view (Figure 8).
- Thickness is based on soil analytical data and shown in Figure 9.
- Assumes October 2003 contamination concentrations have been reduced by 50%.
- Assumes soil contamination detected between 1996 and 1999 has been reduced by 75%.
- Contamination has not impacted groundwater.
- 100 cubic yards of soil removed from the plume area during tank and dispenser removal activities. Actually a total of 270 cubic yards were removed but only 100 cubic yards was removed from the area of the plume footprint (Figures 7 & 8).

The following items likely reduce the mass of contaminants at the site. However, contaminant mass estimate calculations do not include:

- Aeration of intermediate to deep subsurface by staggered well extraction methods.
- Aeration of surface and shallow subsurface during trenching activities.
- Soil removed during the installation of 641 feet of monitoring and extraction well casing

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• Soil removed during the advancement of 650 feet of soil borings

Elevated MtBE levels were detected in the shallow lithology near MW-1 and HP-1 during the 1999 boring and well installation activities. MtBE concentrations from these two sample points attenuated rapidly with depth. The October 2003 soil boring in the same area showed no MtBE remaining in the area. Very low levels of MtBE were detected in the vicinity of HP-5 during the 1999 soil and groundwater investigative activities. The October 2003 soil boring in the same area showed no MtBE remaining in the area.

#### 3.7 Remedial Technologies

An Internal Combustion (IC) system was in operation between February 2002 and January 2003. The IC ran for approximately 290 days and removed about 707 gallons of TPH-G from the vadose zone (Table 9).

A Soil Vapor Extraction and Granulated Activated Carbon (SVE/GAC) system was installed during September 2004 and operated for approximately 183 days during which time about 306 gallons of TPH-G were removed (Table 10).

Approximately 270 cubic yards of soil was removed during tank excavation activities. Approximately 30 cubic yards of soil have been removed as drill cuttings during the installation of monitoring wells, vapor extraction wells, soil borings and GeoProbe boreholes. Additional soil has been removed or aerated during trenching and remedial equipment installation activities. Approximately 500 gallons of contaminated groundwater per year are removed from the site during the development, purging and sampling of groundwater monitoring wells.

This volume of soil cuttings and groundwater removed during investigation activities as well as soil aeration during trenching activates were not used to reduce the mass estimate of contaminants remaining at COE. However, this is additional evidence of the over-cautious nature of the mass estimate calculations.

#### 3.8 BAT

Since the tank and the primary soil contamination source have been removed, eventually background conditions will be achieved in the soil and groundwater at the site. Excavation of the soil surrounding the former USTs and removal of soil boring cuttings were technologies employed to remediate the contamination detected at COE.

Soil vapor extraction methods were employed at the site for approximately 473 days and resulted in the removal of approximately 1,013 gallons of TPH-G from the vadose zone.

#### 3.9 Stockpiled Soil

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No stockpiled soil relating to the former underground storage tanks is stored on this property.

#### 3.10 Monitoring Wells

Five (5) water table and one (1) deep monitoring well as well as four (4) vapor extraction wells are associated with this site and a well construction summary is included as Table 11. Upon issuance of a "No Further Action" letter from the CRWQCB, the monitoring and vapor extraction wells will be properly abandoned under a SJCEHD permit.

Boring logs not used in generating this report may be found in:

- GTI: Soil and Groundwater Investigation Report March 15, 1999
- GTI: Additional Site Characterization Report January 31, 2000
- GTI: Additional Site Characterization Report January 30, 2001
- GTI: Interim Soil Investigation Report October 2, 2003

#### 3.11 Background Conditions

A water quality degradation analysis is summarized below in accordance with § 2550.4(d) of Title 23, California Code of Regulations, Chapter 15:

- 1) Potential adverse effects on groundwater quality and beneficial uses:
  - A. The constituents of concern and average concentrations at the COE site include: The quarterly groundwater monitoring events have revealed that all monitoring wells at the COE site have been non-detect above laboratory reporting limits for all analyzed constituents for the last nine monitoring events.
  - B. Hydrogeological characteristics of the facility and surrounding land are relatively uniform; characterized by alternating layers of sand, silt, and sand-silt mixtures. The details are discussed in Section 2.0.
  - C. Groundwater bearing and slope average N73°W at 0.0019 ft/ft as discussed in Subsection 2.3.2. Groundwater velocity is estimated to be 0.758 to 75.8 feet per year as discussed in Subsection 2.3.4. Vertical groundwater gradient is mostly in the negative direction (downward) at 0.0037 ft/ft, which is similar as the horizontal gradient.
  - D. There are no groundwater users within a 1,600-foot radius of the COE site as discussed in Section 3.1.
  - E. According to the USDA *Soil Survey of San Joaquin County, California* (McElhiney, M. A., 1992); the soils below the site are very deep, somewhat excessively drained, nearly level soil on dunes with 0 to 2 percent slopes. The details are discussed in Subsection 2.2. It is not likely that potential future uses of groundwater in the area will be impacted.
  - F. Background wells show similar pH, EC, ORP, DO and temperature readings to those recorded in wells near the contaminated zone. The source of

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contamination has been removed and it is likely the site will return to background conditions via natural attenuation.

- G. According to the USDA *Soil Survey of San Joaquin County, California* (McElhiney, M. A., 1992); the soils below the site are very deep, somewhat excessively drained, nearly level soil on dunes with 0 to 2 percent slopes. The potential for health risks caused by human exposure (dermal, ingestion or inhalation) is negligible due to unlikely contact with subsurface hydrogeology.
- H. The potential for damage to wildlife, crops, vegetation and physical structures caused by exposure to contaminants is minimal due to the reasons discussed above in Section 3.11G.
- I. The persistence and permanence of the potential adverse effects are finite. It is unlikely that humans or wildlife will come in contact with the residual contaminants. The contaminants have been steadily decreasing with remedial activities and time. Contaminants will likely attenuate to background conditions.
- 2) Potential adverse effects on surface water quality and beneficial uses:
  - A. Mass estimate calculations suggest there may be up to approximately 50 to 100 gallons of TPH-G remaining in the soil beneath COE. The surface areas on and near the site are capped by structures, base rock, concrete or asphalt. Impact to surface water is unlikely.
  - B. Hydrogeological characteristics of the facility and surrounding land are relatively uniform layers of sand-silt mixtures, sands and silts. The details are discussed in Section 2.0.
  - C. Groundwater bearing and slope average N73°W at 0.0019 ft/ft as discussed in Subsection 2.3.2. Groundwater velocity is estimated to be 0.758 to 75.8 feet per year as discussed in Subsection 2.3.4.
  - D. There are no groundwater users within a 1,600-foot radius of the COE site as discussed in Section 3.1. There are no surface waters within a 2,000-foot radius of the COE site.
  - E. According to the USDA *Soil Survey of San Joaquin County, California* (McElhiney, M. A., 1992); the soils below the site are very deep, somewhat excessively drained, nearly level soil on dunes with 0 to 2 percent slopes. The details are discussed in Subsection 2.2. It is not likely that potential future uses of groundwater in the area will be impacted.
  - F. It is unlikely surface water uses will change in the foreseeable future.
  - G. According to the USDA *Soil Survey of San Joaquin County, California* (McElhiney, M. A., 1992); the soils below the site are very deep, somewhat excessively drained, nearly level soil on dunes with 0 to 2 percent slopes. The potential for health risks caused by human, wildlife, crops or vegetation exposure (dermal, ingestion or inhalation) is negligible due to unlikely contact with subsurface hydrogeology.

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H. Surface waters are at such a distance that the potential for health risks caused by human exposure (dermal, ingestion or inhalation) is negligible due to unlikely contact with subsurface hydrogeology.

- I. The potential for damage to wildlife, crops, vegetation and physical structures caused by exposure to contaminants is minimal due to the reasons discussed above in Section 3.11 G.
- J. The persistence and permanence of the potential adverse effects are finite. It is unlikely the contaminants will come in contact with surface waters. It is unlikely that humans or wildlife will come in contact with the contaminants.

#### 3.12 Reports and Information

Unauthorized Release Form (URF), Quarterly Monitoring Reports and other correspondence are on file with SJCEHD and CRWQCB and are not included in this summary report. Additional investigative and characterization reports related to the COE site include:

- GTI: Soil and Groundwater Investigation Report March 15, 1999
- GTI: Additional Site Characterization Report January 31, 2000
- GTI: Soil Vapor Extraction Pilot Test Report August 8, 2000
- GTI: Well Receptor Survey Report November 14, 2000
- GTI: Additional Site Characterization Report January 30, 2001
- GTI: Revised Corrective Action Plan Vadose Zone Remediation dated Feb 26, 2001
- GTI: *Interim Soil Investigation Report* October 2, 2003

#### 3.13 Rationale

For the following reasons, the conditions at this site should not adversely impact water quality, public health, or beneficial use of this property.

#### Site Conditions

- No groundwater contamination has been detected in the last nine quarterly monitoring events.
- The contamination at the site is primarily soil contamination with the bulk being removed by vapor extraction and limited excavation activities.
- The USTs, dispenser islands and primary soil contamination source has been removed.
- There are no domestic, municipal or production wells within at least a 1,600-foot radius for any residual contamination to impact.
- There are no surface waters within at least a 2,000-foot radius for any residual contamination to impact.
- The soil is primarily a mixture of sands and silts. The small amount of remaining contamination will have a tendency to adsorb to the fine-grained silt units, thereby impeding vertical migration.

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• The small amount of residual contamination will likely attenuate to background conditions.

- Portions of the site and adjoining properties not covered with buildings are covered with asphalt or compacted base rock (on-site), thereby limiting vertical migration via filtration.
- Groundwater quality parameters, including DO & ORP measurements, demonstrate that natural attenuation has been active at this site since contaminant release.

#### **TPH-G Contamination**

- An estimated 56 gallons of residual TPH-G contamination remain in the soil. This
  estimate does not include soil removed during investigation activities nor does it
  address natural attenuation.
- The February 16, 2005 groundwater-monitoring event reveals that all of the site's monitoring wells are non-detect above laboratory reporting limits.
- There are no sensitive receptors within at least 1,600-feet of the site
- Portions of the site and adjoining properties not covered by structures are capped by asphalt, compacted base rock or concrete making migration by infiltration unlikely

#### MtBE Contamination

- Historically, MtBE was only detected in one groundwater-monitoring well (MW-1). That monitoring well has been non-detect above laboratory reporting limits for MtBE over the last twelve consecutive quarterly groundwater-monitoring events.
- The most recent soil samples, collected during October 2003, showed no traces of MtBE above laboratory reporting limits.

#### 4.0 LIMITATIONS

This report was prepared in accordance with the generally accepted standard of care and practice in effect at the time Services were rendered. It should be recognized that definition and evaluation of environmental conditions is an inexact science and that the state or practice of environmental geology/hydrology is changing and evolving and that standards existing at the present time may change as knowledge increases and the state of the practice continues to improve. Further, that differing subsurface soil characteristics can be experienced within a small distance and therefore cannot be known in an absolute sense. All conclusions and recommendations are based on the available data and information.

The tasks proposed and completed during this project were reviewed and approved by the local regulatory agency for compliance with the law. No warranty, expressed or implied, is made.

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#### 5.0 SIGNATURES AND CERTIFICATIONS

This report was pr	repared by:
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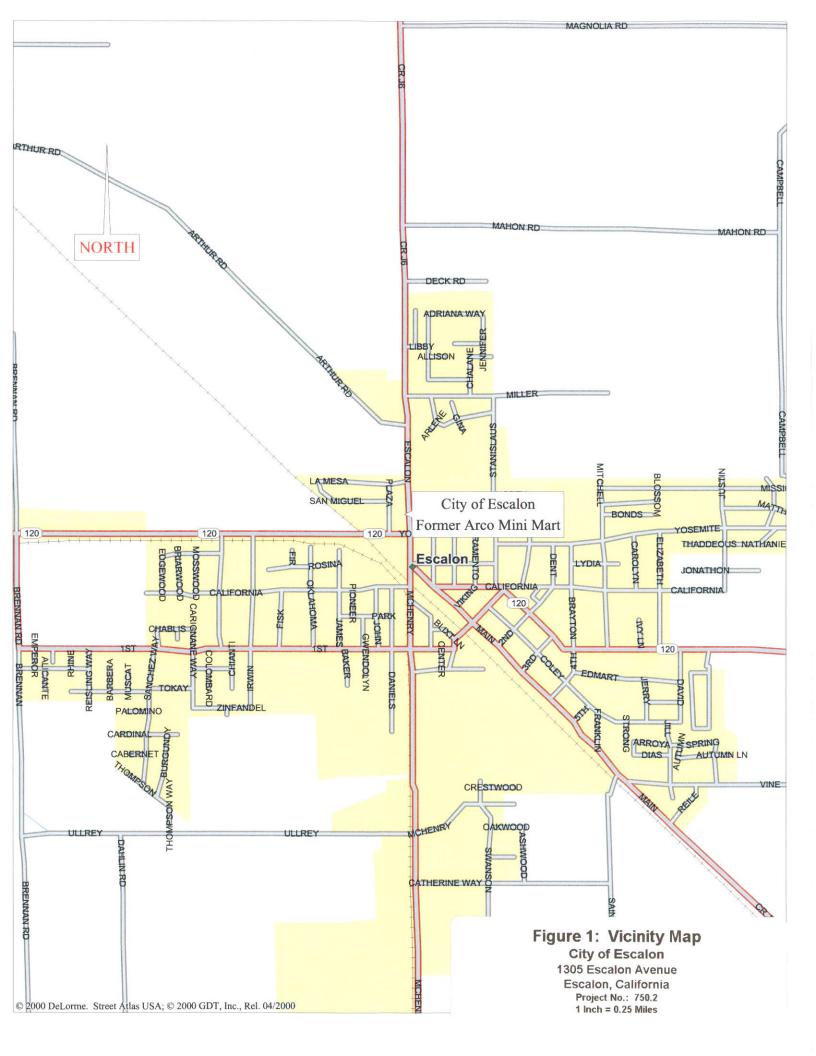
Eric L. Price Geologist

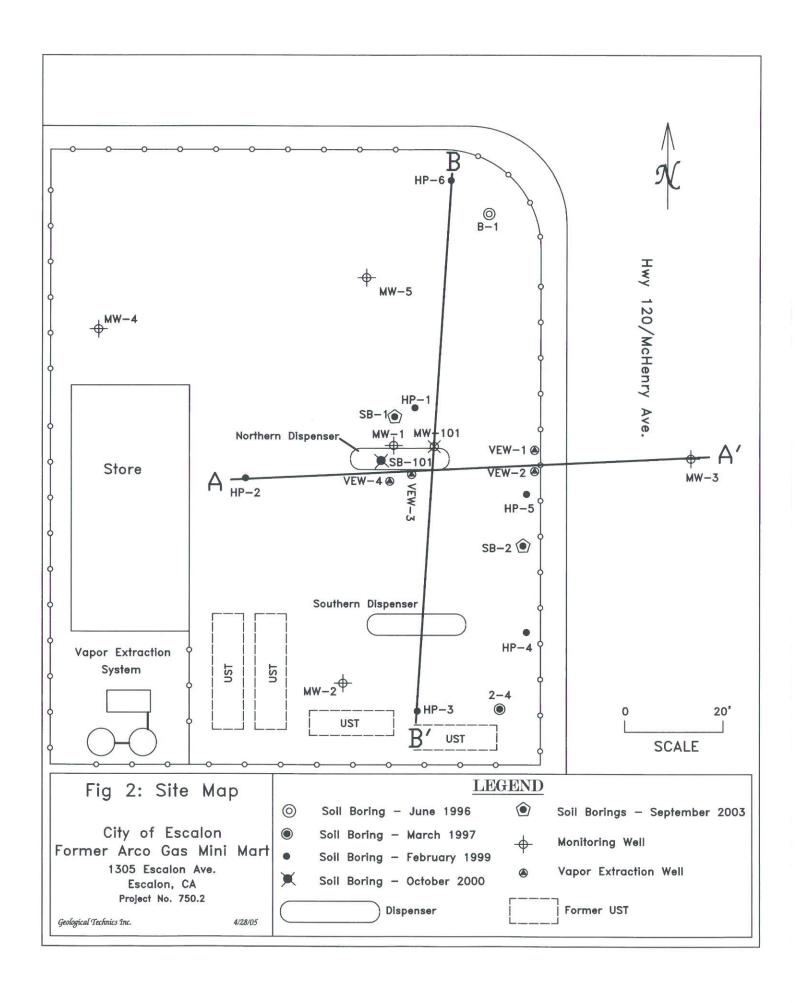
> Raynold Kablanow II, Ph.D. California Professional Geologist #5234 Certified Hydrogeologist #442

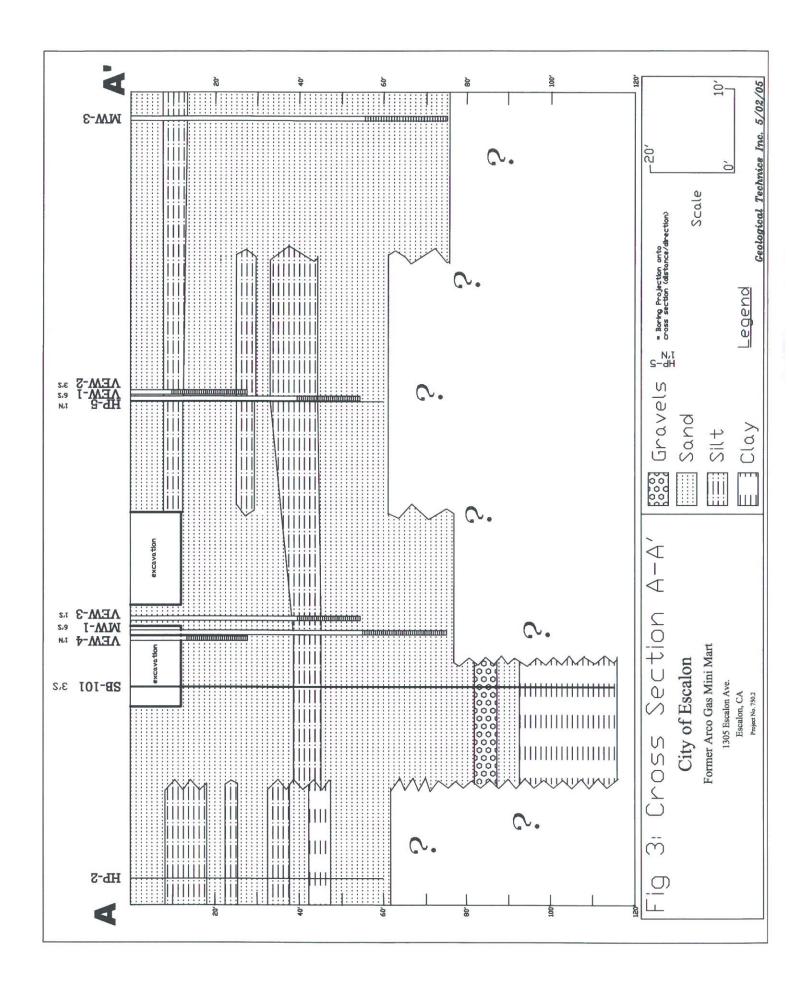


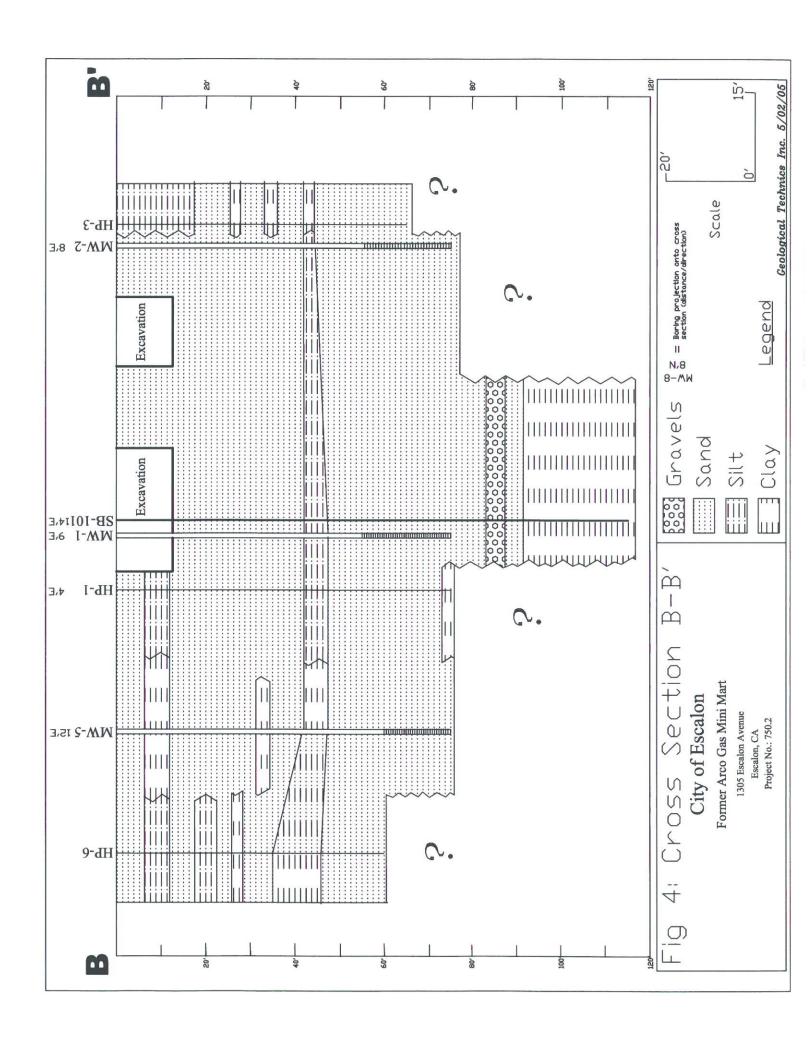
## **Appendix A Summary Tables**

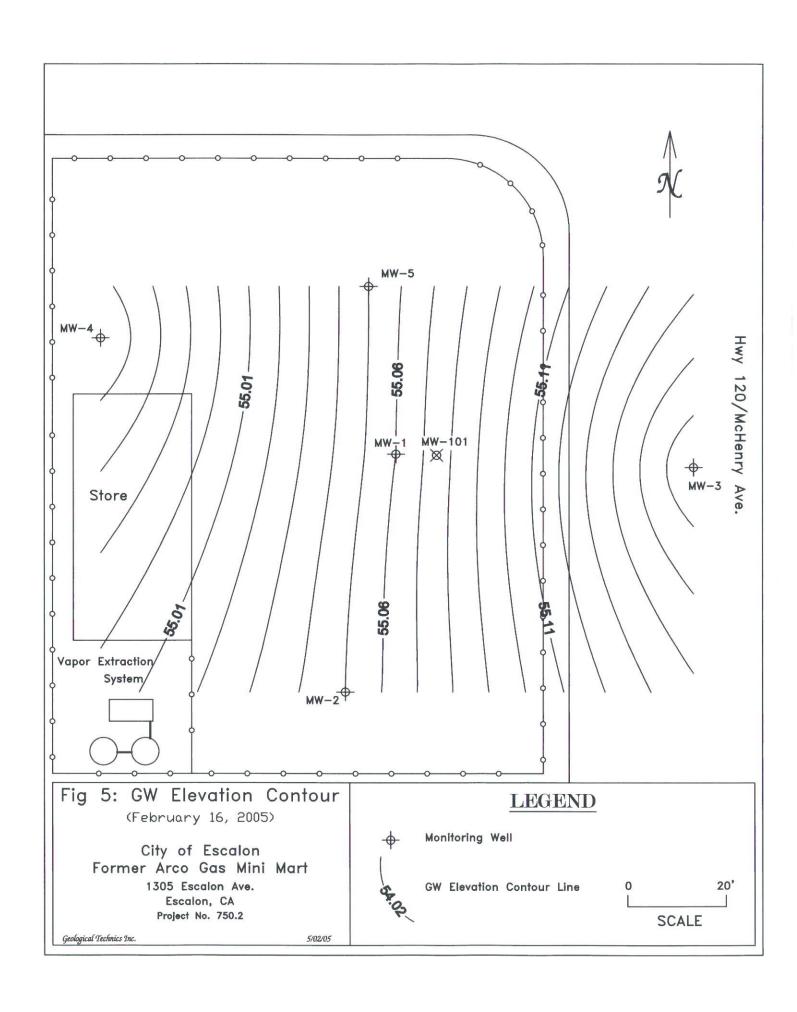
## Appendix B Laboratory Analytical Results

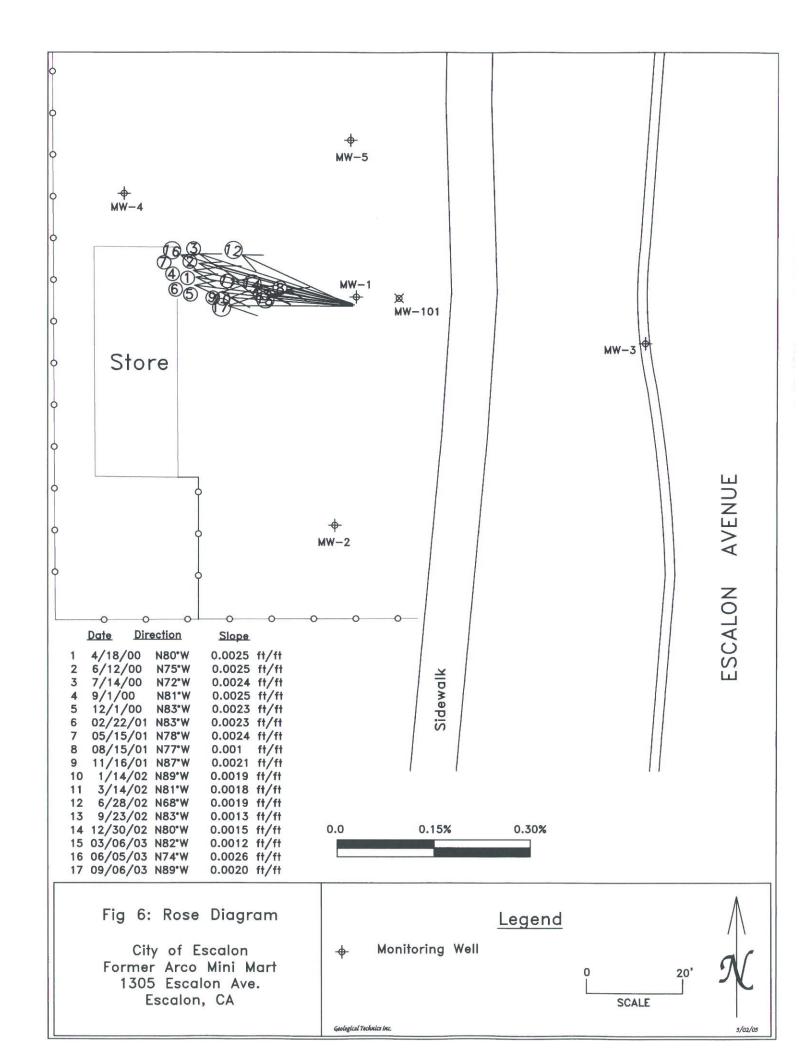


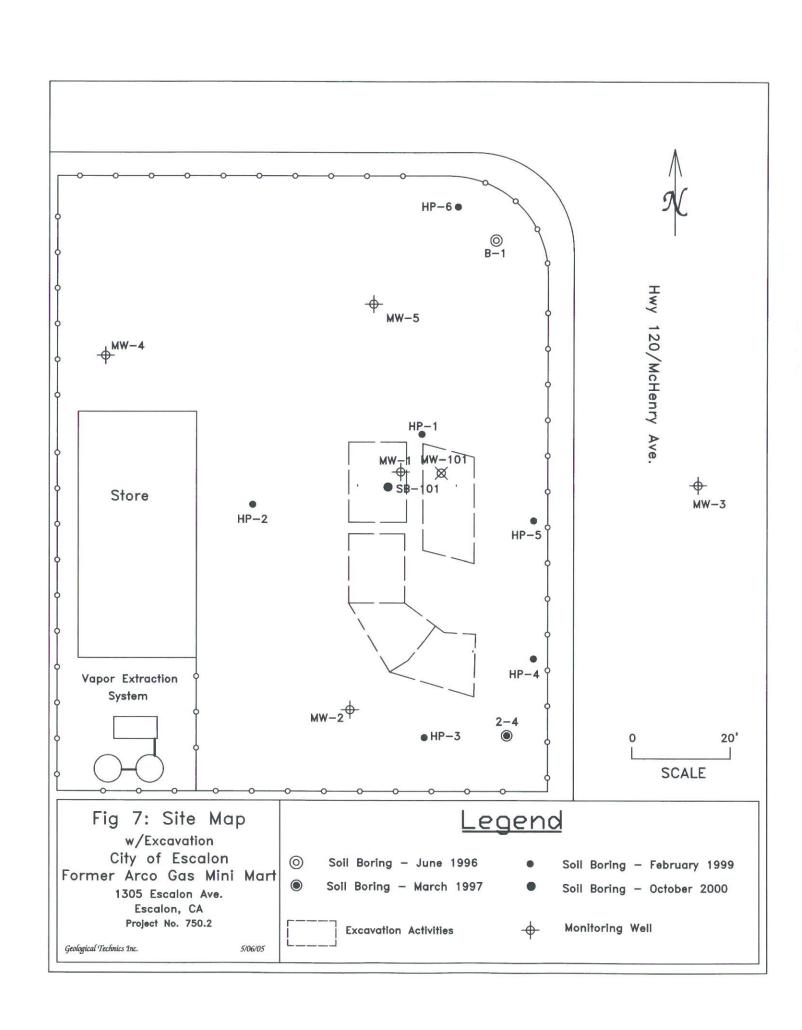


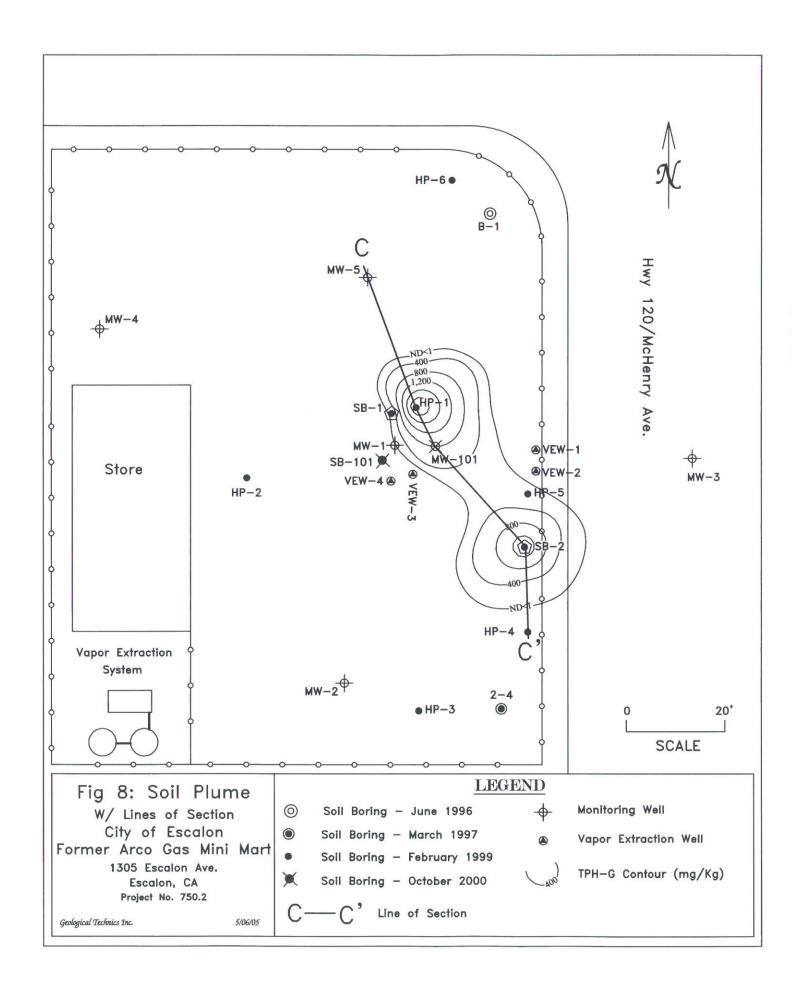


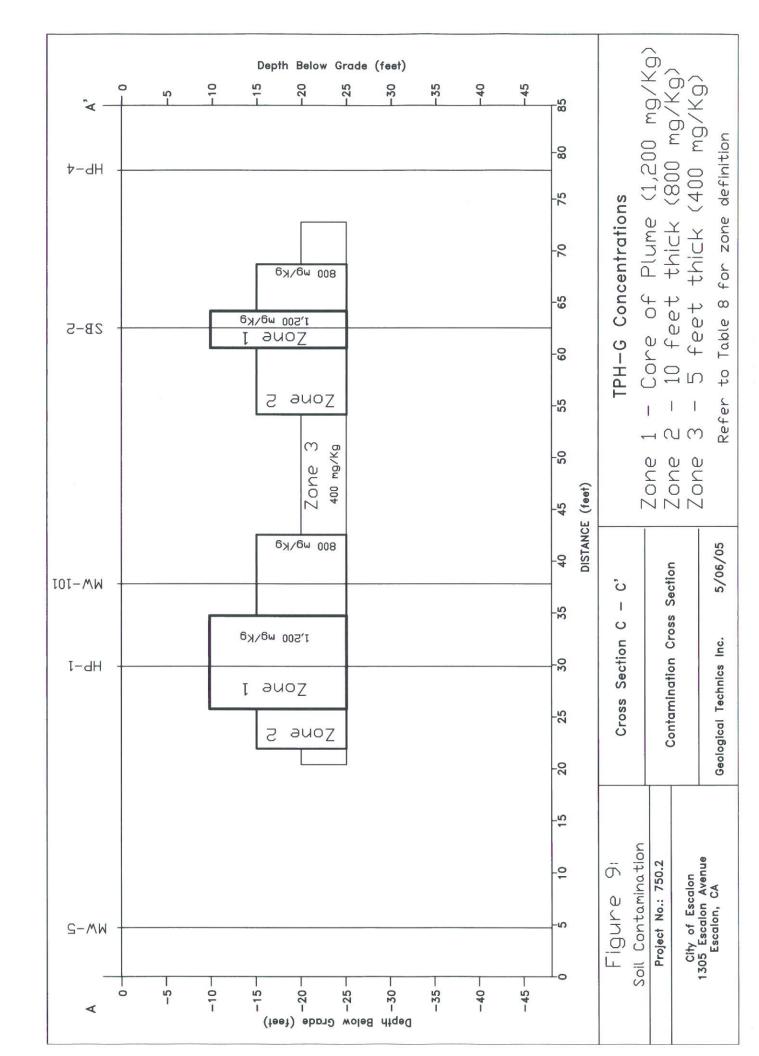












# Table 1: Summary of Groundwater Elevations, Gradients and Bearings

City of Escalon-Former Arco Mini Mart 1305 Escalon Ave. Escalon, CA Project No. 750.2

Date				Elevation	Elevation of Groundwater *	ter *				
	MW-1	MW-2	MW-3	MW-4	MW-5	MW-101	Elevation	DTW	Gradient	Gradient
	GWL Elev.	GWL Elev.	Avg.	Avg.	Bearing	Slope				
04/18/00	56.55	56.56	56.70				26.60	61.49	N80ºW	0.0025
06/12/00	56.70	56.72	56.85				56.76	61.34	N75°W	0.0025
07/14/00	56.39	56.42	56.53				56.45	61.65	N72°W	0.0024
09/01/00	55.75	55.76	55.90				55.80	62.29	N81°W	0.0025
12/01/00	56.16	56.17	56.30	56.13	56.21	55.74	56.19	61.73	N83ºW	0.0023
02/22/01	56.75	56.76	56.89	56.69	56.77	56.50	56.77	61.12	N83°W	0.0023
05/15/01	99.99	56.62	56.75	56.53	56.63	56.38	56.63	61.26	N78°W	0.0024
08/15/01	55.29	55.30	55.44	55.25	55.33	55.06	55.32	62.57	Mo22N	0.0010
11/16/01	54.94	54.93	55.07	54.88	54.97	54.87	54.96	62.90	N87°W	0.0021

Date		Elevatio	on of Groundw	vater (Wells R	esurveyed Acc	cording to AB	Elevation of Groundwater (Wells Resurveyed According to AB 2886 on 1/14/02)	02)		
	MW-1	MW-2	MW-3	WW-4	MW-5	MW-101	Avg. Elev.	DTW	Gradient	Gradient
	GWL Elev.	GWL Elev.	GWL Elev.	GWL Elev.	GWL Elev.	GWL Elev.	Wtr. Table	Avg.	Bearing	Slope
01/14/02	57.72	57.73	57.87	57.65	57.75	57.69	57.74	62.40	S89°W	0.0019
03/14/02	58.17	58.19	58.33	58.12	58.21	58.24	58.20	61.94	N81°W	0.0018
06/28/02	57.70	57.73	57.84	57.63	57.72	57.68	57.72	62.42	N68°W	0.0019
09/23/02	56.13	56.13	56.27	56.09	56.17	56.12	56.16	63.99	N83°W	0.0013
12/30/02	56.94	56.95	57.08	56.88	56.97	56.95	96.99	63.18	N800W	0.0015
03/06/03	57.35	57.35	57.50	57.30	57.38	57.37	57.38	62.77	N82°W	0.0012
06/05/03	56.92	56.95	57.08	26.87	56.96	56.95	96.99	63.19	N74°W	0.0026
60/90/60	55.45	55.43	55.57	55.38	55.50	55.42	55.47	64.68	N89°W	0.0020
12/09/03	55.43	55.47	55.59	55.37	55.49	55.45	55.47	64.67	N62°W	0.0029
10,010	56.40	56 13	26 50	56 30	56.17	56.11	56.16	63.60	NITAOUN	0,000
03/13/04	30.47	20.43	30.39	20.30	70.4/	10.44	20:40	03:03	AA +/AT	0.0023
05/07/04	55.91	55.90	56.07	55.86	55.95	55.92	55.94	64.21	N83°W	0.0028
08/12/04	54.17	54.15	54.30	54.13	54.22	54.17	54.19	65.95	N82°W	0.0022
11/26/04	54.06	54.05	54.21	53.99	54.09	54.06	54.08	90.99	N830W	0.0026
02/16/05	55.06	55.05	55.17	54.96	55.05	55.03	55.06	62:09	N85°W	0.0018
					Histori	Historical Average =	56.71	62.67	N730W	0.0019
						0	١			

Table 2
Vertical Groundwater Gradient Calculations
City of Escalon - Former ARCO Mini Mart
(feet above MSL)

Date 1-Dec-00	Well Pair MW-1 MW-101	Vert Head -0.44	Vert Dist 19.23	Vertical Gradient -0.0228
22-Feb-01	MW-1 MW-101	-0.27	19.52	-0.0138
15-May-01	MW-1 MW-101	-0.24	19.45	-0.0123
15-Aug-01	MW-1 MW-101	-0.24	18.79	-0.0127
16-Nov-01	MW-1 MW-101	-0.09	18.62	-0.0047
14-Jan-02	MW-1 MW-101	-0.05	20.01	-0.0023
14-Mar-02	MW-1 MW-101	0.06	20.23	0.0027
28-Jun-02	MW-1 MW-101	-0.04	20.00	-0.0018
23-Sep-02	MW-1 MW-101	-0.02	19.21	-0.0011
30-Dec-02	MW-1 MW-101	0.00	19.62	-0.0001
6-Mar-03	MW-1 MW-101	0.01	19.82	0.0005
5-Jun-03	MW-1 MW-101	0.01	19.61	0.0005
6-Sep-03	MW-1 MW-101	-0.05	18.87	-0.0024
9-Dec-03	MW-1 MW-101	0.00	18.86	-0.0002
13-Mar-04	MW-1 MW-101	0.00	19.36	-0.0002
7-May-04	MW-1 MW-101	-0.01	19.10	-0.0006
12-Aug-04	MW-1 MW-101	-0.02	18.23	-0.0010
26-Nov-04	MW-1 MW-101	-0.02	18.18	-0.0011
16-Feb-05	MW-1 MW-101	-0.01	18.68	-0.0008

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Table 3: Summary of Analytical Data - Tank and Trench Samples

City Of Escalon 1305 Escalon Ave Escalon, California Project No. 750.2

		_	_	_	_		_	_	
PCE				LN	NT	NT	NT	LN	LN
TBA		mg/kg		ND<200	ND<20	ND<20	ND<20	ND<20	ND<20
TAME		mg/kg		ND<50	ND<5	ND<5	ND<5	ND<5	ND<5
ETBE		mg/kg		ND<50	ND<5	ND<5	ND<5	ND<5	ND<5
DIPE		mg/kg		ND<50	ND<5	ND<5	ND<5	ND<5	ND<5
MTBE		mg/kg		0.54	0.12	6.7	ND<0.01	0.025	80
ТРН	Gasoline	mg/kg			ND<1	ND<1	ND<1	180	6200
Total	Xylenes	mg/kg			0.21	0.051	ND<0.005	12	730
Ethyl	Benzene	mg/kg			ND<0.005	0.0076		3	140
Toluene		mg/kg		-	0.0057	0.055	ND<0.005	2.7	220
Benzene		mg/kg			ND<0.005	0.039	ND<0.005	0.055	2.644
Sample	Depth	Feet		21,	16.5'	13.5'	11.0	19.5	14.5
Sample				Tank1-N	RS-1	RS-2	RS-3	RS-4	RS-5
Date	Sampled			86/60/60	12/09/98	12/09/98	12/09/98	12/09/98	12/09/98
	Sample Sample Benzene Toluene Ethyl Total TPH MTBE DIPE ETBE TAME TBA	Sample Sample Benzene Toluene Ethyl Total TPH MTBE DIPE ETBE TAME TBA TBA Depth Benzene Xylenes Gasoline	Sample Sample Benzene Toluene Ethyl Total TPH MTBE DIPE ETBE TAME TBA TBA TBA Depth Benzene Xylenes Gasoline mg/kg	Sample     Benzene     Total     TPH     MTBE     DIPE     ETBE     TAME     TBA       Depth     Benzene     Xylenes     Gasoline     mg/kg     mg/kg	Sample         Benzene         Ethyl         Total         TPH         MTBE         DIPE         ETBE         TAME         TBA           Image: Tank1-N         Depth         mg/kg         mg/kg <td< td=""><td>Sample         Benzene         Total         TPH         MTBE         DIPE         ETBE         TAME         TBAF         TBAF           Tank1-N         Feet         mg/kg         mg/kg<!--</td--><td>Sample         Sample         Benzene         Total         TPH         MTBE         MTBE         ETBE         TAME         TBA           Tank1-N         Feet         mg/kg         mg/kg&lt;</td><td>Sample         Sample         Benzene         Total         TPH         MTBE         MTBE         DIPE         ETBE         TAME         TBA           Tank1-N         Feet         mg/kg         mg/kg<!--</td--><td>Sample         Sample         Benzene         Total         TPH         MTBE         DIPE         ETBE         TAME         TBM           Tank1-N         Feet         mg/kg         mg/kg&lt;</td></td></td></td<>	Sample         Benzene         Total         TPH         MTBE         DIPE         ETBE         TAME         TBAF         TBAF           Tank1-N         Feet         mg/kg         mg/kg </td <td>Sample         Sample         Benzene         Total         TPH         MTBE         MTBE         ETBE         TAME         TBA           Tank1-N         Feet         mg/kg         mg/kg&lt;</td> <td>Sample         Sample         Benzene         Total         TPH         MTBE         MTBE         DIPE         ETBE         TAME         TBA           Tank1-N         Feet         mg/kg         mg/kg<!--</td--><td>Sample         Sample         Benzene         Total         TPH         MTBE         DIPE         ETBE         TAME         TBM           Tank1-N         Feet         mg/kg         mg/kg&lt;</td></td>	Sample         Sample         Benzene         Total         TPH         MTBE         MTBE         ETBE         TAME         TBA           Tank1-N         Feet         mg/kg         mg/kg<	Sample         Sample         Benzene         Total         TPH         MTBE         MTBE         DIPE         ETBE         TAME         TBA           Tank1-N         Feet         mg/kg         mg/kg </td <td>Sample         Sample         Benzene         Total         TPH         MTBE         DIPE         ETBE         TAME         TBM           Tank1-N         Feet         mg/kg         mg/kg&lt;</td>	Sample         Sample         Benzene         Total         TPH         MTBE         DIPE         ETBE         TAME         TBM           Tank1-N         Feet         mg/kg         mg/kg<

Table 4: Summary of Analytical Data - Soil Borings

City Of Escalon 1305 Escalon Ave Escalon, California Project No. 750.2

Date	Borehole	Sample	Benzene	Toluene	Ethyl	Total	Ethyl Total TPH TEPH	TEPH	MTBE	DIPE	ETBE	TAME	TBA	PCE
Sampled		Depth			Benzene	Xylenes	Gasoline	Diesel	8					
		Feet	ug/Kg	ug/Kg	ng/Kg	ug/Kg	mg/Kg	mg/Kg	ug/Kg	ug/Kg	ug/Kg	ug/Kg	ug/Kg	ug/Kg
06/19/96	B-1	2	ND<5	ND<5	ND<5	ND<5	ND<1	ND<2	ND<50					
		ß	ND<5	ND<5	ND<5	ND<5	ND<1	ND<1	ND<50					
03/19/97	ARCO 2-4	15	ND<5	ND<5	ND<5	ND<5	ND<1	ND<1	ND<50					
		25	ND<5	ND<5	ND<5	ND<5	ND<1	ND<1	ND<50					
		40	ND<5	ND<5	ND<5	ND<5	ND<1	ND<1	ND<50					
		45	ND<5	ND<5	ND<5	ND<5	ND<1	ND<1	ND<50					
		20	ND<5	ND<5	ND<5	ND<5	ND<1	ND<1	ND<50					
02/12/99	HP-1	11-11.5	89	163	14	188	2.0		20,000	ND<500	ND<500	ND<500	8,700	K
		20.5-21	33,700	410,000	160,000	860,000	10,300		58,000	ND/2500	ND/2500	ND/2500	ND/2500 ND<10000	K
		31-31.5	ND<3	5.0	ND<3	9.0	ND<1		360	ND<50	ND/50	ND/50	ND<200	F
		36-36.5	7.0	21	6.0	31	ND<1		810	ND<50	ND<50	ND<50	680	LN.
		46-46.5	611	1,120	146	717	8.0		880	ND<50	ND<50	ND<50	230	LN
		56-56.5	ND<3	4.0	ND<3	5.0	ND<1		16	ND<5	ND<5	ND<5	29	LN
		61-61.5	10	ND<3	ND<3	0.9	ND<1		14	ND<5	ND<5	ND<5	ND<20	Z
02/23/99	HP-2	20.5-21	ND<3	ND<3	ND<3	ND<3	ND<1		ND<5	ND<5	ND<5	ND<5	ND<20	Z
		55.5-56	ND<3	ND<3	ND<3	ND<3	ND<1		ND<5	ND<5	ND<5	ND<5	ND<20	LN
		60.5-61	ND<3	ND<3	ND<3	ND<3	ND<1		19	ND<5	ND<5	ND<5	ND<20	IN
02/23/99	HP-3	20.5-21	ND<3	ND<3	ND<3	ND<3	ND<1		ND<5	ND<5	ND<5	ND<5	ND<20	F
		55.5-56	ND<3	ND<3	ND<3	ND<3	ND<1		ND<5	ND<5	ND<5	ND<5	ND<20	ΙN
		60-60.5	ND<3	ND<3	ND<3	ND<3	ND<1		ND<5	ND<5	ND<5	ND<5	ND<20	IN
02/12/99	HP-4	10.5-11	ND<3	ND<3	ND<3	ND<3	ND<1		8.9	ND<5	ND<5	ND<5	ND<20	Z
		21-21.5	ND<3	ND<3	ND<3	ND<3	ND<1		ND<5	ND<5	ND<5	ND<5	ND<20	N
		36-36.5	ND<3	ND<3	ND<3	ND<3	ND<1		ND<5	ND<5	ND<5	ND<5	ND<20	TN
		45.5-46	ND<3	ND<3	ND<3	ND<3	ND<1		ND<5	ND<5	ND<5	ND<5	ND<20	TN
		56-56.5	ND<3	ND<3	ND<3	ND<3	ND<1		ND<5	ND<5	ND<5	ND<5	ND<20	N
		61-61.5	ND<3	ND<3	ND<3	ND<3	ND<1		ND<5	ND<5	ND<5	ND<5	ND<20	Z
02/12/99	HP-5	21-21.5	6.0	16	4.0	16	ND<1		510	ND<25	ND<25	ND<25	320	L
		35.5-36	ND<3	ND<3	ND<3	4.0	ND<1		27	ND<5	ND<5	ND<5	44	K
		45.5-46	0.9	11	ND<3	12	ND<1		35	ND<5	ND<5	ND<5	21	L
		51-51.5	ND<3	ND<3	ND<3	ND<3	ND<1		ND<5	ND<5	ND<5	ND<5	ND<20	LN
		56-56.5	ND<3	ND<3	ND<3	ND<3	ND<1		5.1	ND<5	ND<5	ND<5	21	6.9
		61-61.5	ND<3	ND<3	ND<3	ND<3	ND<1		9.9	ND<5	ND<5	ND<5	ND<20	Z
02/23/99	HP-6	20.5-21	ND<3	ND<3	ND<3	ND<3	ND<1		ND<5	ND<5	ND<5	ND<5	ND<20	Z
		45.5-46	ND<3	ND<3	ND<3	ND<3	ND<1		ND<5	ND<5	ND<5	ND<5	ND<20	LN
		55.5-56	ND<3	ND<3	ND<3	ND<3	ND<1		ND<5	ND<5	ND<5	ND<5	ND<20	N
		60.5-61	ND<3	ND V3	2003	2/2			NI N	The same of the sa				

Date	Borehole	Sample	Benzene	Toluene	Ethy	Total	TPH	TEPH	MTBE	DIPE	ETBE	TAME	TBA	PCE
Sampled		Depth			Benzene	Xylenes	Gasoline	Diesel						
		Feet	ug/Kg	ug/Kg	ug/Kg	ug/Kg	mg/Kg	mg/Kg	ug/Kg	ug/Kg	ug/Kg	ug/Kg	ug/Kg	ug/Kg
00/00/20	84147 4	30	99	707	90	700	000		0000	OEC. CIA	OF CIA	OBC OIN	AID 4 DOO	FIA
07/30/99	L-WW	25	99	180	97	ec.	3.0		3,200	ND<250	ND<250	ND<250	000,1>UN 052>UN	2
		35	ND<3	4.0	ND<3	0.9	ND<1		2,300	ND<250	ND<250	ND<250	ND<1,000	z
		45	83	18	ND<3	16	ND<1		530	ND<50	ND<50	ND<50	ND<200	Z
		55	ND<3	ND<1	ND<3	0.6	ND<1		7	ND<5	ND<5	ND<5	41	Z
		70	ND<3	ND<1	ND<3	ND<3	ND<1		7	ND<5	ND<5	ND<5	ND<20	LN.
04/29/99	MW-2	15.5-16	ND<5	ND<5	ND<5	ND<5	ND<1		150	ND<5	ND<5	ND<5	ND<20	N
		30.5-31	ND<5	ND<5	ND<5	ND<5	ND<1		ND<5	ND<5	ND<5	ND<5	ND<20	N
		45-45.5	ND<5	ND<5	ND<5	ND<5	ND<1		ND<5	ND<5	ND<5	ND<5	ND<20	F
		60.5-61	ND<5	ND<5	ND<5	ND<5	ND<1		ND<5	ND<5	ND<5	ND<5	ND<20	N
		75.7-76	ND<5	ND<5	ND<5	ND<5	ND<1		ND<5	ND<5	ND<5	ND<5	ND<20	L
06/11/99	MW-3	31-31.5	ND<5	ND<5	ND<5	ND<5	ND<1		ND<50					
		46-46.5	ND<5	ND<5	ND<5	ND<5	ND<1		ND<50					
		61-61.5	ND<5	ND<5	ND<5	ND<5	ND<1		ND<5	ND<5	ND<5	ND<5	ND<20	L
		76-76.5	ND<5	ND<5	ND<5	ND<5	ND<1		ND<50					
04/29/99	VEW-1	15,5-16	ND<5	ND<5	ND<5	ND<5	ND<1		ND<5	ND<5	ND<5	ND<5	ND<20	LN
		25.5-26	ND<5	ND<5	ND<5	5.5	ND<1		ND<5	ND<5	ND<5	ND<5	ND<20	N
		35.5-36	ND<5	ND<5	ND<5	ND<5	ND<1		8	ND<5	ND<5	ND<5	ND<20	TN
		45.5-46	ND<5	ND<5	ND<5	ND<5	ND<1		10	ND<5	ND<5	ND<5	ND<20	LN
		55.5-56	ND<5	ND<5	ND<5	ND<5	ND<1		ND<5	ND<5	ND<5	ND<5	ND<20	N.
10/18/00	MW-4	20.5-21	ND<3	ND<3	ND<3	ND<3	ND<1		ND<50					
		30.5-31	ND<3	ND<3	ND<3	ND<3	ND<1		ND<50					
		50.5-51	ND<3	ND<3	ND<3	ND<3	ND<1		ND<50	1	1	4	000	1
10/19/00	MW-4	60.5-61	ND<3	ND<3	ND<3	ND<3	ND<1		ND<5	ND<5	ND<5	ND<5	ND<20	Z
		70.5-71	ND<3	ND<3	ND<3	ND<3	ND<1		ND<5	ND<5	ND<5	ND<5	ND<20	Z
10/19/00	MW-5	20.5-21	ND<3	ND<3	ND<3	ND<3	ND<1		ND<50					
		30.5-31	ND<3	ND<3	ND<3	ND<3	ND<1		ND<50					
		50.5-51	ND<3	ND<3	ND<3	ND<3	ND<1		ND<50	-	1			
		60.5-61	ND<3	ND<3	ND<3	ND<3	ND<1	*0004	ND<5	ND<5	ND<5	ND<5	ND<20	Z
		00-0:00	CSCIN	CSON	CAUN	CAGN	253	4500	CACIN	CSCIN	CSON	CSON	ואסאכעו	2
10/16/00	SB-101	75.5-76	ND<3	ND<3	ND<3	ND<3	ND<1		ND<50					
		95.5-96	ND<3	ND<3	ND<3	ND<3	ND<1		ND<50				1	
		105.5-106	ND<3	ND<3	ND<3	ND<3	ND<1		ND<5	ND<5	ND<5	ND<5	ND<20	z
10/17/00	SB-101	115-115.5	ND<3	ND<3	ND<3	ND<3	ND<1		ND<5	ND<5	ND<5	ND<5	ND<20	Z
60/90/60	SB-1	19.5	ND<3	ND<3	ND<3	ND<3	ND<1		ND<10	ND<10	ND<10	ND<10	ND<800	L
		44.5	ND<3	ND<3	ND<3	ND<3	ND<1		ND<10	ND<10	ND<10	ND<10	ND<800	L
		54.5	ND<3	ND<3	ND<3	ND<3	ND<1		ND<10	ND<10	ND<10	ND<10	ND<800	IN
60/90/60	SB-2	14.5	ND<1000	1,870	30,400	194,000	3,130		ND<10	ND<10	ND<10	11	3,400	TN
		19.5	9>QN	15.1	8.5	110	20.5		ND<10	ND<10	ND<10	ND<10	ND<800	LN
		34.5	ND<3	ND<3	ND<3	ND<3	ND<1		ND<10	ND<10	ND<10	ND<10	ND<800	N
		44.5	ND<3	ND<3	ND<3	ND<3	ND<1		ND<10	ND<10	ND<10	ND<10	ND<800	Z
		54.5	ND<3	ND<3	ND<3	ND<3	ND<1		ND<10	ND<10	ND<10	ND<10	ND<800	Z

Table 5: Summary of Groundwater Analytical Data

# City of Escalon-Former Arco Mini Mart 1305 Escalon Ave. Escalon, CA Project No. 750.2

Benzene   1	Toluene	Ethyl	Total	TPH	MTBE	ETBE	DIPE	TAME	TBA	EDB	1,2-DCA
ng/L		Benzene	Xylenes	Gasoline	ng/L	ug/L	T/6n	ng/L	ng/L		
		ng/L	ng/L	ng/L							
42		10	57	516	220	ND<5	ND<5	ND<5	ND<20	ND<5	ND<5
10	_	6.0	9	74	23	ND<5	ND<5	ND<5	ND<20		
2		8.0	7	92	62	ND<10	ND<10	ND<10	ND<40		
10		2	15	115	58	ND<5	ND<5	ND<5	ND<20		
14		2	20	163	55	ND<5	ND<5	ND<5	ND<20	ND<5	ND<5
ND<0.3		ND<0.3	ND<0.3	ND<50	71	ND<5	S>QN	ND<5	ND<20		
6.2		96.0	20	72	51	ND<5	ND<5	ND<5	ND<50		
9.9		2.1	30.4	186	6.2	ND<5	ND<5	ND<5	ND<20		
1.6		0.7	9.2	72	80	ND<5	ND<5	ND<5	ND<20		
0.4		9.0	19.4	139	ND<5	ND<5	ND<5	ND<5	ND<20		
ND<0.3	_	ND<0.3	1.2	ND<50	ND<5	ND<5	ND<5	ND<5	ND<20		
ND<0.3	_	ND<0.3	0.3	ND<50	ND<1	ND<5	ND<5	ND<5	ND<10		
ND<0.3 N	Z	ND<0.3	ND<0.3	ND<50	ND<1	ND<5	ND<5	ND<5	ND<10		
ND<0.3 N	Z	ND<0.3	ND<0.3	ND<50	ND<1	ND<5	ND<5	ND<5	ND<20		
ND<0.3 N	Z	ND<0.3	ND<0.3	ND<50	ND<0.5	ND<0.5	ND<0.5	ND<0.5	ND<20		
ND<0.3 N	z	ND<0.3	ND<0.3	ND<50	ND<0.5	ND<0.5	ND<0.5	ND<0.5	ND<20		
Н	z	ND<0.3	ND<0.3	ND<50	ND<0.5	ND<0.5	ND<0.5	ND<0.5	ND<20		
ND<0.3 N	Z	ND<0.3	ND<0.3	ND<50	ND<0.5	ND<0.5	ND<0.5	ND<0.5	ND<20		
ND<0.3 N	_	ND<0.3	ND<0.3	ND<50	ND<0.5	ND<0.5	ND<0.5	ND<0.5	ND<20		
ND<0.3 N	~	ND<0.3	ND<0.3	ND<50	ND<0.5	ND<0.5	ND<0.5	ND<0.5	ND<20		
ND<0.5 N	z	ND<0.5	ND<1	ND<50	IN	NT	N	IN	IN		
-	- [1		0.0	4		4	1	4	000	4	
	_	ND<0.3	ND<0.3	ND<50	ND<5	ND<5	ND<5	ND<5	ND<20	ND<5	ND<5
ND<0.3	_	ND<0.3	ND<0.3	ND<50	ND<5	ND<5	ND<5	ND<5	ND<20		
ND<0.3   N	_	ND<0.3	ND<0.3	ND<50	ND<5	ND<5	ND<5	ND<5	ND<20		
ND<0.3   N	_	ND<0.3	ND<0.3	ND<50	ND<5	ND<5	ND<5	ND<5	ND<20		
ND<0.3	-	ND<0.3	ND<0.3	ND<50	ND<5	ND<5	ND<5	ND<5	ND<20	ND<5	ND<5
ND<0.3	_	ND<0.3	ND<0.3	ND<50	ND<5	ND<5	ND<5	ND<5	ND<20		
$\vdash$		ND<0.3	9.0>QN	ND<50	ND<5	ND<5	ND<5	ND<5	ND<50		
ND<0.3	_	ND<0.3	ND<0.3	ND<50	ND<5	ND<5	ND<5	ND<5	ND<20		

4
0
N
8
6
2
50

5/2/2005

Wells	Date	Benzene	Toluene	Ethyl	Total	TPH	MTBE	ETBE	DIPE	TAME	TBA	EDB	1,2-DCA
		ng/L	ng/L	Benzene	Xylenes	Gasoline	ng/L	ng/L	ng/L	ng/L	ng/L		
				ng/L	ng/L	ng/L							
MW.2	03/11/02	ND-03	ND-03	ND-03	ND-03	NDVEO	ND/A	A/OIN	ND.	A CIN	ND.20		
Z-AA IAI	06/08/02	ND-ON	S C C C C C C C C C C C C C C C C C C C	NDVO.3	NDVO.3	ND/50	S S S S S S S S S S S S S S S S S S S	S S S S S S S S S S S S S S S S S S S	S A CIN	S A CIN	NDS-SU		
	09/23/02	ND<0.3	ND<0.3	ND<0.3	ND<0.3	ND<50	ND<5	ND<5	ND<5	ND<5	ND<20		
	12/30/02	ND<0.3	ND<0.3	ND<0.3	ND<0.3	ND<50	ND<1	ND<5	ND<5	ND<5	ND<10		
	03/06/03	ND<0.3	ND<0.3	ND<0.3	ND<0.3	ND<50	ND<1	ND<5	ND<5	ND<5	ND<10		
	06/05/03	ND<0.3	ND<0.3	ND<0.3	ND<0.3	ND<50	ND<1	ND<5	ND<5	ND<5	ND<20		5
	60/90/60	ND<0.3	ND<0.3	ND<0.3	ND<0.3	ND<50	ND<0.5	ND<0.5	ND<0.5	ND<0.5	ND<20		
	12/09/03	ND<0.3	ND<0.3	ND<0.3	0.3	ND<50	ND<0.5	ND<0.5	ND<0.5	ND<0.5	ND<20		
	03/13/04	ND<0.3	ND<0.3	ND<0.3	ND<0.3	ND<50	ND<0.5	ND<0.5	ND<0.5	ND<0.5	ND<20		
	05/07/04	ND<0.3	ND<0.3	ND<0.3	ND<0.3	ND<50	ND<0.5	ND<0.5	ND<0.5	ND<0.5	ND<20		
	08/12/04	ND<0.3	ND<0.3	ND<0.3	ND<0.3	ND<50	ND<0.5	ND<0.5	ND<0.5	ND<0.5	ND<20		
	11/26/04	ND<0.3	ND<0.3	ND<0.3	ND<0.3	ND<50	ND<0.5	ND<0.5	ND<0.5	ND<0.5	ND<20		
	02/16/05	ND<0.5	ND<0.5	ND<0.5	ND<1	ND<50	N	LN	N	TN	M		
MW-3	04/18/00	ND<0.3	ND<0.3	ND<0.3	ND<0.3	ND<50	ND<5	ND<5	ND<5	ND<5	ND<20	ND<5	ND<5
	07/14/00	ND<0.3	ND<0.3	ND<0.3	ND<0.3	ND<50	ND<5	ND<5	ND<5	ND<5	ND<20		
	09/01/00	ND<0.3	ND<0.3	ND<0.3	ND<0.3	ND<50	ND<5	ND<5	ND<5	ND<5	ND<20		
	12/01/00	ND<0.3	ND<0.3	ND<0.3	ND<0.3	ND<50	ND<5	ND<5	ND<5	ND<5	ND<20		
	02/22/01	ND<0.3	ND<0.3	ND<0.3	ND<0.3	ND<50	ND<5	ND<5	ND<5	ND<5	ND<20	ND<5	ND<5
	05/15/01	ND<0.3	ND<0.3	ND<0.3	ND<0.3	ND<50	ND<5	ND<5	ND<5	ND<5	ND<20		
	08/15/01	ND<0.3	ND<0.3	ND<0.3	ND<0.6	ND<50	ND<5	ND<5	ND<5	ND<5	ND<50		
	08/15/01	ND<0.3	ND<0.3	ND<0.3	ND<0.3	ND<50	ND<5	ND<5	ND<5	ND<5	ND<20		
	03/14/02	ND<0.3	ND<0.3	ND<0.3	ND<0.3	ND<50	ND<5	ND<5	ND<5	ND<5	ND<20		
	06/28/02	ND<0.3	ND<0.3	ND<0.3	ND<0.3	ND<50	ND<5	ND<5	ND<5	ND<5	ND<20		
	09/23/02	ND<0.3	ND<0.3	ND<0.3	ND<0.3	ND<50	ND<5	ND<5	ND<5	ND<5	ND<20		
	12/30/02	ND<0.3	ND<0.3	ND<0.3	ND<0.3	ND<50	ND<1	ND<5	ND<5	ND<5	ND<10		
	03/06/03	ND<0.3	ND<0.3	ND<0.3	ND<0.3	ND<50	ND<1	ND<5	ND<5	ND<5	ND<10		
	06/05/03	ND<0.3	ND<0.3	ND<0.3	ND<0.3	ND<50	ND<1	ND<5	ND<5	ND<5	ND<20		
	60/90/60	ND<0.3	ND<0.3	ND<0.3	ND<0.3	ND<50	ND<0.5	ND<0.5	ND<0.5	ND<0.5	ND<20		
	12/09/03	ND<0.3	ND<0.3	ND<0.3	ND<0.3	ND<50	ND<0.5	ND<0.5	ND<0.5	ND<0.5	ND<20		
	03/13/04	ND<0.3	ND<0.3	ND<0.3	ND<0.3	ND<50	ND<0.5	ND<0.5	ND<0.5	ND<0.5	ND<20		
	05/07/04	ND<0.3	ND<0.3	ND<0.3	ND<0.3	ND<50	ND<0.5	ND<0.5	ND<0.5	ND<0.5	ND<20		
	08/12/04	ND<0.3	ND<0.3	ND<0.3	ND<0.3	ND<50	ND<0.5	ND<0.5	ND<0.5	ND<0.5	ND<20		
	11/26/04	ND<0.3	ND<0.3	ND<0.3	ND<0.3	ND<50	ND<0.5	ND<0.5	ND<0.5	ND<0.5	ND<20		
	02/16/05	ND<0.5	ND<0.5	ND<0.5	ND<1	ND<50	N	N	N	N	Z		
MW-4	12/01/00	ND<0.3	ND<0.3	ND<0.3	ND<0.3	ND<50	ND<5	ND<5	ND<5	ND<5	ND<20		
	02/22/01	ND<0.3	ND<0.3	ND<0.3	ND<0.3	ND<50	ND<5	ND<5	ND<5	ND<5	ND<20	ND<5	ND<5

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roject No. 7

		ng/L	ng/L	Benzene	Xylenes	Gasoline	ng/L	ng/L	ng/L	ng/L	ng/L		
				ng/L	ng/L	ng/L							
MW-4	05/15/01	ND<0.3	ND<0.3	ND<0.3	ND<0.3	ND<50	ND<5	ND<5	ND<5	ND<5	ND<20		
	08/15/01	ND<0.3	ND<0.3	ND<0.3	9.0>QN	ND<50	ND<5	ND<5	ND<5	ND<5	ND<50		
	11/16/01	ND<0.3	ND<0.3	ND<0.3	ND<0.3	ND<50	ND<5	ND<5	ND<5	ND<5	ND<20		
	03/14/02	ND<0.3	ND<0.3	ND<0.3	ND<0.3	ND<50	ND<5	ND<5	ND<5	ND<5	ND<20		
	06/28/02	ND<0.3	ND<0.3	ND<0.3	ND<0.3	ND<50	ND<5	ND<5	ND<5	ND<5	ND<20		
	09/23/02	ND<0.3	ND<0.3	ND<0.3	ND<0.3	ND<50	ND<5	ND<5	ND<5	ND<5	ND<20		
	12/30/02	ND<0.3	ND<0.3	ND<0.3	ND<0.3	ND<50	ND<1	ND<5	ND<5	ND<5	ND<10		
	60/90/60	ND<0.3	ND<0.3	ND<0.3	ND<0.3	ND<50	ND<1	ND<5	ND<5	ND<5	ND<10		
	06/05/03	ND<0.3	ND<0.3	ND<0.3	ND<0.3	ND<50	ND<1	ND<5	ND<5	ND<5	ND<20		
	60/90/60	ND<0.3	ND<0.3	ND<0.3	ND<0.3	ND<50	ND<0.5	ND<0.5	ND<0.5	ND<0.5	ND<20		
	12/09/03	ND<0.3	ND<0.3	ND<0.3	ND<0.3	ND<50	ND<0.5	ND<0.5	ND<0.5	ND<0.5	ND<20		
	03/13/04	ND<0.3	ND<0.3	ND<0.3	ND<0.3	ND<50	ND<0.5	ND<0.5	ND<0.5	ND<0.5	ND<20		
	05/07/04	ND<0.3	0.5	ND<0.3	0.7	ND<50	ND<0.5	ND<0.5	ND<0.5	ND<0.5	ND<20		
	08/12/04	ND<0.3	ND<0.3	ND<0.3	ND<0.3	ND<50	ND<0.5	ND<0.5	ND<0.5	ND<0.5	ND<20		
	11/26/04	ND<0.3	ND<0.3	ND<0.3	ND<0.3	ND<50	ND<0.5	ND<0.5	ND<0.5	ND<0.5	ND<20		
	02/16/05	ND<0.5	ND<0.5	ND<0.5	ND<1	ND<50	IN	NT	IN	TN	TN		
MW-5	12/01/00	ND<0.3	ND<0.3	ND<0.3	ND<0.3	177	ND<5	ND<5	ND<5	ND<5	ND<20		
	02/22/01	ND<0.3	ND<0.3	ND<0.3	ND<0.3	209	ND<5	ND<5	ND<5	ND<5	ND<20	ND<5	ND<5
	05/15/01	ND<0.3	ND<0.3	ND<0.3	ND<0.3	354	ND<5	ND<5	ND<5	ND<5	ND<20		
	08/15/01	ND<0.3	ND<0.3	ND<0.3	ND<0.6	ND<50	ND<5	ND<5	ND<5	ND<5	ND<50		
	11/16/01	ND<0.3	ND<0.3	ND<0.3	ND<0.3	ND<50	6.1	ND<5	ND<5	ND<5	ND<20		
	03/14/02	ND<0.3	ND<0.3	ND<0.3	ND<0.3	ND<50	ND<5	ND<5	ND<5	ND<5	ND<20		
	06/28/02	ND<0.3	ND<0.3	ND<0.3	ND<0.3	ND<50	ND<5	ND<5	ND<5	ND<5	ND<20		
	09/23/02	ND<0.3	ND<0.3	ND<0.3	ND<0.3	ND<50	ND<5	ND<5	ND<5	ND<5	ND<20		
	12/30/02	ND<0.3	ND<0.3	ND<0.3	ND<0.3	ND<50	ND<1	ND<5	ND<5	ND<5	ND<10		
	03/06/03	ND<0.3	ND<0.3	ND<0.3	ND<0.3	ND<50	ND<1	ND<5	ND<5	ND<5	ND<10		
	06/05/03	ND<0.3	ND<0.3	ND<0.3	ND<0.3	ND<50	ND<1	ND<5	ND<5	ND<5	ND<20		
	60/90/60	ND<0.3	ND<0.3	ND<0.3	ND<0.3	ND<50	ND<0.5	ND<0.5	ND<0.5	ND<0.5	ND<20		
	12/09/03	ND<0.3	ND<0.3	ND<0.3	ND<0.3	ND<50	ND<0.5	ND<0.5	ND<0.5	ND<0.5	ND<20		
	03/13/04	ND<0.3	ND<0.3	ND<0.3	ND<0.3	ND<50	ND<0.5	ND<0.5	ND<0.5	ND<0.5	ND<20		
	05/07/04	ND<0.3	ND<0.3	ND<0.3	ND<0.3	ND<50	ND<0.5	ND<0.5	ND<0.5	ND<0.5	ND<20		
	08/12/04	ND<0.3	ND<0.3	ND<0.3	ND<0.3	ND<50	ND<0.5	ND<0.5	ND<0.5	ND<0.5	ND<20		
	11/26/04	ND<0.3	ND<0.3	ND<0.3	ND<0.3	ND<50	ND<0.5	ND<0.5	ND<0.5	ND<0.5	ND<20		
	02/16/05	ND<0.5	ND<0.5	ND<0.5	ND<1	ND<50	¥	Z	Ā	N N	Į.		
MW-101	12/01/00	e	45	14	84	852	54	ND<5	ND<5	ND<5	ND<20		
	02/22/01	ND<0.3	0.4	ND<0.3	60	7.	ND	ND/5	ND	ND	ND-20	ND/5	ND/5

5/2/2005

Date Ber	Bei	Benzene	Toluene	Ethyl	Total	TPH	MTBE	ETBE	DIPE	TAME	TBA	EDB	1,2-DCA
ug/L   ug/L   Ben;	ng/L		Ben:	Benzene	Xylenes	Gasoline	ng/L	ug/L	ng/L	ng/L	ug/L		
ng/L	/bn	/bn	/bn	_	ng/L	ng/L							
05/15/01   ND<0.3   ND<0.3	ND<0.3	-	ND<0	6.0	ND<0.3	ND<50	ND<5	ND<5	ND<5	ND<5	ND<20		
08/15/01 ND<0.3 ND<0.3 ND<0.3	ND<0.3		ND<0	6	9.0>QN	ND<50	ND<5	ND<5	ND<5	ND<5	ND<50		
11/16/01 ND<0.3 ND<0.3 ND<0.3	ND<0.3	$\vdash$	ND<0.	3	ND<0.3	ND<50	ND<5	ND<5	ND<5	ND<5	ND<20		
03/14/02   ND<0.3   ND<0.3   ND<0.3	ND<0.3		ND<0.3		ND<0.3	ND<50	ND<5	ND<5	9>QN	ND<5	ND<20		
06/28/02   ND<0.3   ND<0.3   ND<0.3	ND<0.3		ND<0.3		ND<0.3	ND<50	ND<5	ND<5	S>QN	ND<5	ND<20		
09/23/02   ND<0.3   ND<0.3   ND<0.3	ND<0.3	H	ND<0.3		ND<0.3	ND<50	ND<5	ND<5	S>QN	S>QN	ND<20		
12/30/02   ND<0.3   ND<0.3   ND<0.3	ND<0.3		ND<0.3		ND<0.3	ND<50	ND<1	ND<5	ND<5	S>QN	ND<10		
03/07/03   ND<0.3   ND<0.3   ND<0.3	ND<0.3	H	ND<0.3		ND<0.3	ND<50	ND<1	ND<5	ND<5	ND<5	ND<10		
06/05/03   ND<0.3   ND<0.3   ND<0.3	ND<0.3	_	ND<0.3		ND<0.3	ND<50	ND<1	ND<5	ND<5	ND<5	ND<20		
09/06/03   ND<0.3   ND<0.3	ND<0.3		ND<0.3		ND<0.3	ND<50	ND<0.5	ND<0.5	ND<0.5	ND<0.5	ND<20		
12/09/03   ND<0.3   ND<0.3	ND<0.3	_	ND<0.3		ND<0.3	05>QN	ND<0.5	ND<0.5	ND<0.5	ND<0.5	ND<20		
03/13/04   ND<0.3   ND<0.3   ND<0.3	ND<0.3	_	ND<0.3		ND<0.3	ND<50	ND<0.5	ND<0.5	ND<0.5	ND<0.5	ND<20		
05/07/04   ND<0.3   ND<0.3   ND<0.3	ND<0.3	$\vdash$	ND<0.3		ND<0.3	ND<50	ND<0.5	ND<0.5	ND<0.5	ND<0.5	ND<20		
08/12/04   ND<0.3   ND<0.3   ND<0.3	ND<0.3	H	ND<0.3		ND<0.3	ND<50	ND<0.5	ND<0.5	ND<0.5	ND<0.5	ND<20		
11/26/04   ND<0.3   ND<0.3   ND<0.3	ND<0.3	H	ND<0.3		ND<0.3	ND<50	ND<0.5	ND<0.5	ND<0.5	ND<0.5	ND<20		
02/16/05   ND<0.5   ND<0.5   ND<0.5	ND<0.5	_	ND<0.5		ND<1	ND<50	LN.	Z	LN	LN	N		

ND= non detect. N/A=Not tested. ug/L=micrograms per liter(parts per billion)

Table 6: Summary of Groundwater Parameters

#### City of Escalon 1305 Escalon Avenue Escalon, California Project No. 750.2

Monitoring Well			MW-1					MW-2					MW-3		
	рН	E.C.	٥F	ORP	DO	pН	E.C.	°F	ORP	DO	рН	E.C.	°F	ORP	DO
Date															
04/18/00				118					165					156	
07/14/00				173					172					184	
02/22/01				65					88					190	
05/15/01				83					88					118	
08/15/01				156					160					118	
11/16/01				66					85					129	
03/14/02	7.11	742	66.6	82		7.80	651	66.6	99		7.16	731	67.6	190	
06/28/02	7.12	699	68.2	156		7.18	602	67.8	111.5		7.17	669	68.2	112.3	
09/23/02	7.38	640	68.9	50		7.27	619	68.4	62.1		7.30	719	72.0	89.4	
12/30/02	7.21	663	66.6	38.3		7.27	579	66.6	33.1		7.04	701	66.6	30.6	
03/06/03	7.20	697	67.1	55		7.09	537	66.92	67		7.05	717	67.1	49	
06/06/03	7.37	716	67.5	87	1.86	7.39	556	67.46	92	1.73	7.50	733	67.64	81	2.51
09/06/03	7.41	733	68.2	45	3.98	7.52	663	68.9	34.7	4.16	7.35	754	67.1	54.1	4.82
12/09/03	7.19	717	65.5	115.1	4.02	7.41	680	66.38	99.2	3.45	7.20	766	66.02	112	3.37
03/13/04	7.56	636	66.9	23.9	4.21	7.61	542	67.28	23.5	4.10	7.36	652	67.28	14.7	6.38
05/07/04	7.14	682	67.5	28.8	5.23	7.25	580	67.46	34.3	4.52	7.12	701	67.28	33.1	5.18
08/12/04	7.03	562	67.3	92.0	2.40	7.17	602	67.46	82	3.20	7.03	690	67.82	48	5
11/26/04	7.72	592	66.4	60.5	3.67	7.79	601	66.02	53.4	3.80	7.80	611	66.2	56.8	4.52
02/16/05	7.00	834	66.7	247	4.10	7.14	670	65.84	219	4.10	7.00	811	66.38	227	3.70

Monitoring Well			MW-4					MW-5					MW-10	1	
	рН	E.C.	°F	ORP	DO	рН	E.C.	°F	ORP	DO	pН	E.C.	°F	ORP	DO
Date															
04/18/00															
07/14/00															
02/22/01				68					87					42	
05/15/01				63					71					74	
08/15/01				175					170					224	
11/16/01				63					62				1	68	
03/14/02	7.08	490	66.6	65		6.99	777	66.7	44		8.12	583	66.6	42	
06/28/02	7.06	683	67.8	93.2		6.94	669	67.8	98.1		7.26	515	67.8	86.8	
09/23/02	7.15	707	68.4	69.9		7.2	584	68.7	49.6		7.46	549	68.7	66.5	
12/30/02	7.08	653	66.7	41.4		7.01	564	66.9	40.0		7.35	547	66.4	35.2	
03/06/03	7.14	725	66.7	89		7.06	584	67.1	80		7.37	559	66.6	41	
06/06/03	7.34	726	67.1	87	2.30	7.24	628	67.28	90	2.00	7.47	581	67.1	84	1.87
09/06/03	7.24	722	67.5	90.2	4.17	7.17	636	68	64.9	4.22	7.54	639	67.6	44.3	4.02
12/09/03	7.34	588	66.2	70	3.80	7.20	553	66.38	102	3.51	7.42	610	66.0	101.4	3.28
03/13/04	7.10	618	67.1	23.5	4.20	7.25	539	67.46	23.6	3.88	7.52	524	67.1	21.9	4.17
05/07/04	7.25	640	67.5	40.7	7.25	7.24	584	67.64	39.9	4.74	7.27	558	67.5	21.2	4.25
08/12/04	6.97	550	68.0	74	3.10	6.98	508	67.82	82	3.00	7.25	512	67.3	81	2.8
11/26/04	8.43	226	66.9	29.8	3.98	7.89	362	67.28	50.8	3.53	7.79	533	66.9	56.7	3.89
02/16/05	6.90	763	66.7	235	3.60	6.90	649	67.1	236	3.70	7.12	655	66.4	220	3.50

Table 7: 2001 Contaminant Mass Estimate Calculations (TPH-G)

City of Escalon - Former Arco Mini Mart
1305 Escalon Avenue
Project No. 750.2

cont.	1	3.7	1.2	cont.	kg	2.23	4491.80	9904.41	1597.49
conv. c		0.000001	0.000001	cont. load c	kg/L	0.000001705	kg =	= <b>q</b> I	gal =
cont. load ma/ka	1,154	1.333	0.5	cont. load****	mg/L	1.705	total		
conv.	0.4536	0.4536	0.4536	vol H2O	liters	1310139			
density ** Ibs/ft3	110	110	120	vol of H20***	ft3	46267			
volume ft3	77885	56200	44370	volume	ft3	132192			
area *		2248		area *	(ft.)	4896			
matrix thickness	25	25	15		depth - ft thickness	27			
depth - ft	0-25	25 - 50	50 - 65		depth - ft	65 - 89			
matrix	sand & silt	sand & silt	sand	matrix	type	water			
zone	#	#2	#3		zone				

<sup>\* =</sup> Area calculated by CAD software. Excavation volume of 270 cubic yards of soil subtracted from Zone 1.

\*\* = estimated from Watson and Burnett, 1995

\*\*\* Vol. H2O =volume of zone x porosity (30%)

\*\*\*average zone concentration

Table 8: 2005 Contaminant Mass Estimate Calculations (TPH-G)

City of Escalon - Former Arco Mini Mart
1305 Escalon Avenue
Project No. 750.2

		9/	28	158 348 56
cont.				
conv. mg/kg	0.000001	0.000001	0.000001	kg = lb = gal =
cont. load mg/kg	1,200	800	400	total
conv. Ibs/kg	0.4536	0.4536	0.4536	
density ** lbs/ft3	110	110	110	
volume ft3	400	1900	2900	
area * (ft.)	160	250	009	
thickness	15	10	5	
depth - ft	10 to 25	15 to 25	20 to 25	
matrix	sand & silt	sand & silt	sand & silt	
zone	#1	#2	#3	

<sup>\* =</sup> Area calculated by CAD software. Excavation volume of 270 cubic yards of soil subtracted from Zone 1.

\*\* = estimated from Watson and Burnett, 1995

Vol. H2O =volume of zone x porosity (30%)

Table 9: Gallons of TPH-Gas removed by Internal Combustion Engine (I.C.)

City of Escalon 1305 Escalon, Ave. Escalon, CA Project No.: 750.3

LC Startup 2/5/2002 10:08 0 2/14/2002 9:54 0 2/27/2002 10:35 IC Shutdown to high emmisions.	Cum. Days 0.00 8.99 22.02 misions.	period	# 110/1/					ab data	Concentration	ALL LICA	LIOW (CTM)	2		מאוו מכונים	dallons
I.C Startup 2/5/2002 10:08 2/14/2002 9:54 2/27/2002 10:35 IC Shutdown to high emmisic	0.00 8.99 22.02 ons. 22.02 22.02 22.03		# 10 //	(mdd)	* (mdd)	Period	(mdd)	(mg/l)	(mg/L)	(ctm)	for Period	lbs./day	Cum. lbs.	gal/day	removed
1.C Startup 2/5/2002 10:08 2/14/2002 9:54 2/27/2002 10:35 IC Shutdown to high emmisic	0.00 8.99 22.02 ons.														
2/5/2002 10:08 2/14/2002 9:54 2/27/2002 10:35 IC Shutdown to high emmisic IC Restart	0.00 8.99 22.02 22.02 22.02 29.93														
2/14/2002 9:54 2/27/2002 10:35 IC Shutdown to high emmisic IC Restart	8.99 22.02 ons. 22.02 29.93		ဗ	301	1204		1100	4.6		9					
2/27/2002 10:35 IC Shutdown to high emmisic IC Restart	22.02 ons. 22.02 29.93 48 11		က	257	1028					35					
IC Shutdown to high emmisic	22.02 29.93	22.02	က	96	384	872			3.62	45	47	15.2	334	2.4	54
IC Restart	22.02 29.93														
00.04 0000/14	22.02														
4/22/2002 13:00	29.93		4							25					
4/30/2002 10:44	48 11		4	863	3452		4900	20		20					
5/18/2002 15:10	-	26.09	4							20	22	39.0	1,351	6.3	218
I.C. Failed nite of the 18th															
I.C. Restart															
6/14/2002 17:10	48.11		4							50					
6/18/2002 7:45	51.72		4	525	2100		2400	9.80		32					
7/18/2002 9:19	81.78		4	326	1304		1300	5.50		20					
8/14/2002 8:30	108.75	60.64	4	346			1000	4.30	6:53	45	44	26.0	2,927	4.2	472
8/14/2002 8:30	108.75			346			1000	4.30		45					
	142.70		4	342			610	2.50		38					
10/25/2002 11:35	180.88		4	364			610	2.50		55					
	200.96		4	435			480	2.00		50					
12/10/2002 8:30	226.75	118.00	4	228			360	1.50	2.56		47	10.8	4,203	1.7	678
Shut VETS down (Spike Test)	st)														
VETS Restart															
	226.75		4	197											
	226.79		4	238			320	1.30		20					
	227.64		4	185			450	1.90		45					
1/27/2003 8:00	252.64		4	134			210	0.89		45					
1/31/2003 8:35	256.66	29.91	4	168					1.40	20	48	0.9	4,381	1.0	707
I.C. Restart															
VETS Restart															
12/9/2003 8:45	256.66		182	18.5			210	0.87		47					
12/10/2003 12:32	257.82		1&2	18.5			18	0.07		47					
12/23/2003 5:00	270.50		182	17.9			18	0.07		45					
1/14/2004 9:00	292.67		1 thru 4	14.9					0.34	55	49	1.5	4,381	0.2	707

\* OVM readings adjusted by a factor of 4.0 from 2/5/02 thru 12/22/01 to bring them into line with lab data.

Table 10: Gallons of TPH-Gas Removed by SVE System

City of Escalon 1305 Escalon, Ave. Escalon, CA Project No.: 750.2

	-		Action	Adinoton	AVO OVA			Ava Vanor		Avo Air			Vanor	2
ŏ	days in	Vapor	OVM	MVO	for	Lab data	ab data Lab data	O	Air Flow	Flow (CFM)	removal		extracted	gallons
Cum. Days   pe	period	Well #	(mdd)	* (vmdd)	Period	(ppmv)	(mg/L)	(mg/L)	(ctm)	for Period	lbs./day	Cum. lbs.	gal/day	removed
H													0.00	
0.0		1,2,3,4 (30%)	36.9	48.9		99	0.230		182					
3.0		1,2 (50%) 3,4 (20%)	42.8	56.7					195					
10.0		1,2 (50%) 3,4 (20%)	19.6	26.0		26	0.100		185					
19.0		3,4 (100%)	41.3						183					
26.0		3,4 (100%) 1,2 (10%)	74.3	98.4		110	0.440		160					
31.0	31.0	1,2 (60%) 3,4 (40%)	63.2	83.7	61.4			0.257	160	177.5	4.0	123	9.0	20
40.0		3,4 (100%)	46.7	61.9					180					
46.0		1,2 (35%) 3,4 (50%)	32.3	42.8					140					
59.1		1,2 (10%) 3,4 (60%)	689	91.3		29	0.270		128					
67.3	27.3	2,4 (100%)	232.9	308.6	126.1			0.270	120	142.0	3.4	215	0.5	55
System Down for Modifications 11/30/04 thru 12/16/04	2/16/04													
67.3														
71.5		1 thru 4 (100%)	57.5	76.2					185					
85.4		1,2 (50%) 3,4 (50%)	37.8	50.1					168					
85.4		3,4 (100%)	68.7	91.0		83	0.340		155					
98.4		3,4 (100%)	2.99	88.4		98	0.350		151	200 000				
109.3	45.0	1,2 (100%) 3,4 (20%)	27.5	36.4	68.4			0.345	149	161.6	4.9	420	0.8	122
116.3		3,4 (100%)	85.6	113.4					130					
121.3		1 thru 4 (50%)	47.2	62.5					135					
127.3		3,4 (100%)	58.3	77.2					138					
134.3		3,4 (100%)	68.4	90.6		80	0.330		132					
140.6	24.3	1,2 (100%)	8.1	10.7	70.9			0.330	140	135.0	3.9	514	9.0	205
147.3		3 4 (100%)	519	68.8					129					
157.1		3.4 (100%)	49.8			56	0.230		140					
164.3		3,4 (100%)	55.2						140					
170.4		3,4 (100%)	61.3											
183.4	36.1	3,4 (100%)	63.9		74.8	29	0.280	0.255	140	137.3	3.1	625	0.5	306

\* OVM readings adjusted by a factor of 1.325 to bring them into line with lab data.

# Table 11: Summary of Well Construction

## City of Escalon-Former Arco Mini Mart 1305 Escalon Ave. Escalon, CA Project No. 750.2

		_	_	_	_		_	_	_	_	_	_
Grout Seal	υ		S	3	က	S	S	S	5	5	S	S
Grou	From		50	51	51	58	55.5	83	36	6.5	35	∞
ır Seal	To		50	51	51	58	55.5	83	36	6.5	35	00
Annular Seal	From		53	53	53	09	58	98	38	8.5	37	10
Pack	То	53		53	53	09	58	98	38	8.5	37	10
Filter Pack	From	75		75	75	78	75	68	55	27	55	27
creen	То	55		55	55	63	09	85	40	10	39	12
Well Screen	From	75		75	75	78	75.0	87	55	27	54	27
Sand Type		#3	#3	#3	#3	#3	#3	#3	Pea Gravel	Pea Gravel	Pea Gravel	Pea Gravel
Slot Size		0.020	0.020	0.020	0.020	0.020	0.020	0.020	0.040	0.040	0.040	0.040
Casing Type		PVC	PVC	PVC	PVC	PVC	PVC	PVC	PVC	PVC	PVC	PVC
Well Casing Diameter	(III)	2	2	2	2	2	2	2	4	4	4	4
Boring Diameter	(III)	8.5	10	8	8	8	8	9	10	10	10	10
Total Depth (ft)		75		75	9/	80	92	95	55	27	55	27
Date Drilled		7/20/1000	1130/1999	4/29/1999	6/11/1999	10/18/2000	10/19/2000	10/18/2000	4/29/1999	4/29/1999	7/30/1999	7/30/1999
Status												
Well/Boring Number		MW 1	[N] W - I	MW-2	MW-3	MW-4	MW-5	MW-101	VEW-1	VEW-2	VEW-3	VEW-4
Well/Boring Type		Monitonia	MOIIIOIIII	Monitoring	Monitoring	Monitoring	Monitoring	Monitoring	Vapor Extraction	Vapor Extraction	Vapor Extraction	Vapor Extraction



#### Air Toxics Ltd. Introduces the Electronic Report

Thank you for choosing Air Toxics Ltd. To better serve our customers, we are providing your report by e-mail. This document is provided in Portable Document Format which can be viewed with Acrobat Reader by Adobe.

This electronic report includes the following:

- · Work order Summary;
- · Laboratory Narrative;
- · Results; and
- · Chain of Custody (copy).

AN ENVIRONMENTAL ANALYTICAL LABORATORY

#### **WORK ORDER #:** 0504240

Work Order Summary

CLIENT:

Mr. Project Manager

Geological Technics Inc.

1101 7th Street

Modesto, CA 95354

BILL TO:

Mr. Accounts Payable

Geological Technics Inc.

1101 7th Street

Modesto, CA 95354

PHONE:

209-522-4119

P.O. #

086285E

FAX:

209-522-4227

PROJECT#

750.2 COE (ARCO)

DATE RECEIVED: DATE COMPLETED: 04/13/2005 04/26/2005

CONTACT:

Taryn Badal

FRACTION #	NAME
01A	Effluent
02A	Influent
03A	Lab Blank
04A	LCS
04B	LCS

RECEIPT VAC./PRES.
Tedlar Bag
Tedlar Bag
NA
NA
NA

CERTIFIED BY:

Sinda d. Fruman

04/26/05

Laboratory Director

Certification numbers: AR DEQ - 03-084-0, CA NELAP - 02110CA, LA NELAP/LELAP- AI 30763, NJ NELAP - CA004 NY NELAP - 11291, UT NELAP - 9166389892

Name of Accrediting Agency: NELAP/Florida Department of Health, Scope of Application: Clean Air Act, Accreditation number: E87680, Effective date: 07/01/04, Expiration date: 06/30/05

Air Toxics Ltd. certifies that the test results contained in this report meet all requirements of the NELAC standards

This report shall not be reproduced, except in full, without the written approval of Air Toxics Ltd.

180 BLUE RAVINE ROAD, SUITE B FOLSOM, CA - 95630 (916) 985-1000 . (800) 985-5955 . FAX (916) 985-1020

#### LABORATORY NARRATIVE Modified TO-3

#### Geological Technics Workorder# 0504240

Two 1 Liter Tedlar Bag samples were received on April 13, 2005. The laboratory performed analysis for volatile organic compounds in air via modified EPA Method TO-3 using gas chromatography with photo ionization and flame ionization detection. The method involves concentrating up to 200 mL of sample. The concentrated aliquot is then dry purged to remove water vapor prior to entering the chromatographic system. The TPH (Gasoline Range) results are calculated using the response factor of Gasoline and correspond to the range of hydrocarbons from C5 to C10. A molecular weight of 100 is used to convert the TPH (Gasoline Range) ppmv result to ug/L.

See the data sheets for the reporting limits for each compound.

Method modifications taken to run these samples include:

Requirement	TO-3	ATL Modifications
Daily Calibration Standard Frequency	Prior to sample analysis and every 4 - 6 hrs	Prior to sample analysis and after the analytical batch = 20 samples</td
Initial Calibration Calculation	4-point calibration using a linear regression model	5-point calibration using average Response Factor
Initial Calibration Frequency	Weekly	When daily calibration standard recovery is outside 75 - 125 %, or upon significant changes to procedure or instrumentation
Moisture Control	Nafion system	Sorbent system
Minimum Detection Limit (MDL)	Calculated using the equation DL = A+3.3S, where A is intercept of calibration line and S is the standard deviation of at least 3 reps of low level standard	40 CFR Pt. 136 App. B
Preparation of Standards	Levels achieved through dilution of gas mixture	Levels achieved through loading various volumes of the gas mixture

#### **Receiving Notes**

There were no receiving discrepancies.

#### **Analytical Notes**

There were no analytical discrepancies.

#### **Definition of Data Qualifying Flags**

Seven qualifiers may have been used on the data analysis sheets and indicate as follows:

- B Compound present in laboratory blank greater than reporting limit.
- J Estimated value.

- E Exceeds instrument calibration range.
- S Saturated peak.
- Q Exceeds quality control limits.
- U Compound analyzed for but not detected above the detection limit.
- M Reported value may be biased due to apparent matrix interferences.

File extensions may have been used on the data analysis sheets and indicates as follows:

- a-File was requantified
- b-File was quantified by a second column and detector
- r1-File was requantified for the purpose of reissue

### **Summary of Detected Compounds MODIFIED EPA METHOD TO-3 GC/PID/FID**

Client Sample ID: Effluent

Lab ID#: 0504240-01A

Compound	Rpt. Limit (ppmv)	Rpt. Limit (uG/L)	Amount (ppmv)	Amount (uG/L)
Benzene	0.0040	0.013	0.046 M	0.15 M
Toluene	0.0040	0.015	0.41 M	1.6 M
Ethyl Benzene	0.0040	0.017	0.018	0.080
Total Xylenes	0.0040	0.017	0.058	0.25
TPH (Gasoline Range)	0.10	0.41	16	63
Methyl tert-butyl ether	0.0040	0.014	0.0051	0.018

Client Sample ID: Influent

Lab ID#: 0504240-02A

	Rpt. Limit	Rpt. Limit	Amount	Amount
Compound	(ppmv)	(uG/L)	(ppmv)	(uG/L)
Toluene	0.037	0.14	1.0	3.8
Ethyl Benzene	0.037	0.16	1.5	6.5
Total Xylenes	0.037	0.16	15	65
TPH (Gasoline Range)	0.92	3.8	67	280

Client Sample ID: Effluent Lab ID#: 0504240-01A

#### MODIFIED EPA METHOD TO-3 GC/PID/FID

File Name:	d041318	Date of Collection: 4/12/05
Dil. Factor:	4.00	Date of Analysis: 4/13/05 07:12 PM

Compound	Rpt. Limit (ppmv)	Rpt. Limit (uG/L)	Amount (ppmv)	Amount (uG/L)
Benzene	0.0040	0.013	0.046 M	0.15 M
Toluene	0.0040	0.015	0.41 M	1.6 M
Ethyl Benzene	0.0040	0.017	0.018	0.080
Total Xylenes	0.0040	0.017	0.058	0.25
TPH (Gasoline Range)	0.10	0.41	16	63
Methyl tert-butyl ether	0.0040	0.014	0.0051	0.018

M = Reported value may be biased due to apparent matrix interferences.

Container Type: 1 Liter Tedlar Bag

		Method
Surrogates	%Recovery	Limits
Fluorobenzene (FID)	122	75-150
Fluorobenzene (PID)	107	75-125

Client Sample ID: Influent Lab ID#: 0504240-02A

#### MODIFIED EPA METHOD TO-3 GC/PID/FID

File Name:	d041317	Date of Collection: 4/12/05
Dil. Factor:	37.0	Date of Analysis: 4/13/05 06:31 PM

Compound	Rpt. Limit (ppmv)	Rpt. Limit (uG/L)	Amount (ppmv)	Amount (uG/L)
Benzene	0.037	0.12	Not Detected	Not Detected
Toluene	0.037	0.14	1.0	3.8
Ethyl Benzene	0.037	0.16	1.5	6.5
Total Xylenes	0.037	0.16	15	65
TPH (Gasoline Range)	0.92	3.8	67	280
Methyl tert-butyl ether	0.037	0.13	Not Detected	Not Detected

#### Container Type: 1 Liter Tedlar Bag

		Method
Surrogates	%Recovery	Limits
Fluorobenzene (FID)	118	75-150
Fluorobenzene (PID)	103	75-125

#### Client Sample ID: Lab Blank Lab ID#: 0504240-03A

#### MODIFIED EPA METHOD TO-3 GC/PID/FID

File Name: Dil. Factor:	d041303 1.00		Date of Collection: No. 10 Date of Analysis: 4/	
Compound	Rpt. Limit (ppmv)	Rpt. Limit (uG/L)	Amount (ppmv)	Amount (uG/L)
Benzene	0.0010	0.0032	Not Detected	Not Detected
Toluene	0.0010	0.0038	Not Detected	Not Detected
Ethyl Benzene	0.0010	0.0043	Not Detected	Not Detected
Total Xylenes	0.0010	0.0043	Not Detected	Not Detected
TPH (Gasoline Range)	0.025	0.10	Not Detected	Not Detected
Methyl tert-butyl ether	0.0010	0.0036	Not Detected	Not Detected
Container Type: NA - Not Applicable				
Surrogates		%Recovery		Method Limits
Fluorobenzene (FID)		118		75-150
Fluorobenzene (PID)		105		75-125

#### Client Sample ID: LCS Lab ID#: 0504240-04A

#### MODIFIED EPA METHOD TO-3 GC/PID/FID

File Name:	d041325b	Date of Co	ollection: NA
Dil. Factor:	1.00	Date of A	nalysis: 4/13/05 11:26 PM
Compound			%Recovery
Benzene			103
Toluene			90
Ethyl Benzene			88
Total Xylenes			93
Methyl tert-butyl ether			77
Container Type: NA - Not A	pplicable		
			Method
Surrogates		%Recovery	Limits
Fluorobenzene (PID)		106	75-125

Client Sample ID: LCS Lab ID#: 0504240-04B

#### MODIFIED EPA METHOD TO-3 GC/PID/FID

File Name: Dil. Factor:	d041324 1.00		Collection: NA Analysis: 4/13/05 10:51 PM
		Date of	Allalysis: 4/13/05 10:51 PWI
Compound			%Recovery
TPH (Gasoline Range)			82
Container Type: NA - Not App	licable		
Cumanatas		0/ <b>D</b>	Method
Surrogates		%Recovery	Limits
Fluorobenzene (FID)		128	75-150

0504240 Page tot

## Geological Technics Inc.

1101 7th Street
Modesto, CA
(209) 522-4119 Fax 522-427
C-mail: #1@peological pachinist.cc



Chain of Custody

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